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TECHNICAL REPORT: NAVTRAEQUIPCEN IH-338

HELMET MOUNTED DISPLAY FEASIBILITY MODEL

John H. Allen and Richard C. Hebb
Advanced Simulation Concepts Laboratory
Naval Training Equipment Center
Orlando, Florida 32813

FINAL REPORT February 1983

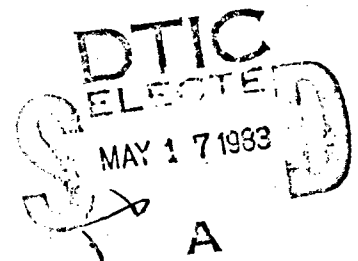
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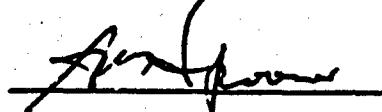
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direction of the observer. Since the computer image generator requires a measureable period of time to create an image for a specific head pointing direction, an undesirable display orientation error is induced each time the viewer moves his head. A method of continuously compensating for this image display error was provided and is described. This feasibility model has demonstrated successfully, on a small scale, the helmet mounted display concept. This concept will be utilized in a full scale development model scheduled for delivery under contract in 1985.

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SECTION I

CONSIDERATIONS FOR A VISUAL SIMULATION

In general, the need for improved high resolution, wide field of view displays in visual simulation systems exists because of the increasing necessity for training combat missions in flight simulators. Total duplication of the rich visual environment present everywhere outside the cockpit during actual nap of the earth missions or any other low level mission, though, is not possible using current visual simulation technology. Nor, in all probability, will it ever be. Due to technological and physical restrictions a visual display is only a representation or simulation of the actual visual environment. The choice of what should be simulated and how it should be done is not easy due to the number, nature and variety of visual cues available to and used by a veteran pilot during the performance of an actual mission. Until our understanding of the human visual system and its interactions with the real world are more complete, visual simulation systems will be designed to provide as much realism and fidelity as is possible with available funding and technology. Under these conditions, it seems reasonable to conclude that a display which provides eye limited resolution and high detail over the entire available field of view will supply the essential elements of a fully adequate visual simulation system.¹

Typically, a high resolution, wide field of view display is created by butting together several computer generated video displays. Each display is separately created by a single image generator channel feeding video to either a video projector or to a conventional CRT monitor. The displayed video image is derived from a digital representation of a mathematically modeled landscape or gaming area depicting the training scene. This digital portrayal is more simply known as a data base. Depending upon the particular training requirements, the data base may be modeled from existing terrain information from some known location or, it can be entirely fictitious. In the usual case, then, a wide field of view visual simulation system consists of a number of video displays and their associated computer image generator channels, each channel obtaining visual information from a common data base. For a given area of visual display, or equivalently, field of view, increasing the number of the video displays and image generator channels improves the resolution of the whole display and increases the quantity of detail available to the viewer. Unfortunately, the visual simulation is improved at the expense of doing so with a more costly, complicated visual simulator system.

Another method of providing a wide field of view display with high resolution and detail utilizes a movable high resolution inset display. Two prin-

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1. Statler, Irving C. Characteristics of Flight Simulator Visual Systems, NASA, Washington, DC 20546 and U.S. Army Aviation Research and Development Command, St. Louis, MO 93166. NASA Tm.-81 278, or AVRAD COM Technical Report 81-A-8, April 1981, pp. 1, 2, 56, 57.

cial types are target tracked (moved to follow some displayed target) and head/eye tracked (moved to follow the observer's head and eye position).

A target tracked display is usually projected upon or inset into a background low resolution, wide field of view display. In this way, imagery for the entire visual simulation can be furnished by a two-channel image generator, one channel driving the movable high resolution display, the other sourcing the low resolution background display. The position of the target tracked display that is within the background display is a function of target location. In other words, the display is servo driven in some manner so as to place a target image in the proper position within the background display. Target imagery can consist of an enemy missile site or even an accompanying friendly aircraft. Its visual content is entirely dependent upon the simulated mission. The advantages of this visual simulation system is that it provides some of the benefits of wide field of view and high resolution using a limited number of image generation channels. The primary disadvantage to such a system is that each additional high resolution object/target that is to be displayed requires still another target tracked high resolution display and image generator. As a result of this constraint, a target tracked display may be inefficient for certain kinds of training tasks.

A head/eye tracked display is tracked or moved about in direct response to the trainee's head and eye pointing direction. The visual display appears only where the observer happens to be looking. Further, if the display area is large enough to cover the observer's field of view, a visual simulation can appear to take place throughout the available viewing volume of the simulator, while in fact, the actual display covers only the immediate area available to the viewer. If a second smaller display, also head and eye tracked, is inserted at the center of the display mentioned above, high resolution imagery can be made available to the viewer along his line of sight. Since the human visual system detects high resolution imagery only in the small central foveal region of the eye, proper design of a two-channel head/eye tracked visual display results in the illusion that a high resolution, wide field of view visual simulation is omnipresent.

When the NAVAIR funded Helmet Mounted Display task started in 1978, its primary goal was to determine the feasibility of developing a fully operational dual channel, head/eye tracked, pilot helmet mounted display. Through the efforts of an in-house team a preliminary prototype or feasibility model was designed and built. Successfully demonstrated at a preproposal conference in November 1981, the feasibility model served as a test bed for many concepts, some of which were included in the specifications for the advanced development model, the Visual Display Research Tool, now in the procurement cycle.²

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2. For additional information on the advanced development model, see articles entitled "Helmet Mounted Laser Projector" in the Proceedings of the 1981 Image Generation Display Conference II (AFHRL) and the 3rd Interservice/Industry Training Equipment Conference.

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The Visual Display Research Tool, 6.3 funded by NAVAIP, is targeted for incorporation into the Visual Technology Research Simulator (VTRS) in early 1985. This advanced visual simulation system contains only two computer generated displays, yet it provides both a wide angle field of view and high resolution. The high resolution inset display contains high detail scene content and is presented only at the observer's point of gaze or, equivalently, area of interest. The surrounding low resolution display, containing low detail scene content, fills the remainder of the observer's field of view. Visually, the composite display will tend to match the acuity profile of the human eye by generating high resolution imagery only along the foveal axis, and low resolution imagery in the periphery.

An artist's concept of the proposed system is depicted in Figure 1. The flight simulator cockpit is enclosed by a spherical screen. Two displays are projected onto the highly retro-reflective interior surface of the sphere. The scenes in both the high resolution Area of Interest (AOI) display and the surrounding Instantaneous Field of View (IFOV) display are computer generated according to the pilot's line of sight. His line of sight, with reference to the ground, at any one moment in time, is a consequence of his cockpit referenced head and eye position, as well as the attitude and position of the simulated aircraft. Each display is an interlaced video raster composed of 1023 horizontal scan lines. Instead of being projected by a conventional high resolution video projector, though, they are formed from video modulated laser beams which are projected and scanned from the pilot's helmet.

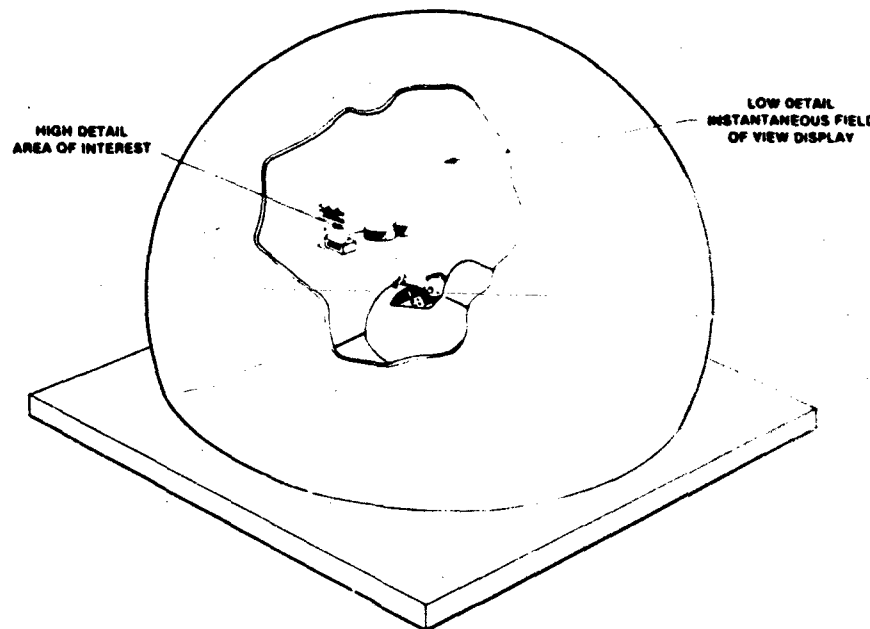


Figure 1. Artist's Concept of an Area of Interest, Instantaneous Field of View Dome Display.

A computer image generator channel generates a blue, a green and a red video signal to form the full color visual scene within each display. Six video signals are required for the two displays, two of each color. Each of the video signals drives an acousto optic modulator. The six acousto optic modulators, in turn, modulate the intensity of two blue and two green laser beams from a remotely located argon laser, and two red laser beams from a companion dye laser. The three modulated, red, green, and blue laser beams that form each of the two displays are optically combined so as to create a single composite full color, beam for each display. Each of the two composite beams are then arranged so as to strike the facets of a rotating high speed scanner mirror. Here the composite beams for each display are horizontally line scanned. After being formed, the line scans for each display are then suitably focused onto the polished ends of two coherent flat fiber optic ribbon cables for subsequent relay to the helmet mounted projector.

The far end of each flat fiber optic ribbon is attached to the pilot's helmet. There, the two separate, full color line scans emerge and are vertically frame scanned by oscillating scanner mirrors as they are projected onto the interior surface of the spherical screen.

The display that the pilot/trainee's attention will be most focused upon, the Area of Interest (AOI), will occupy a viewing area of approximately 25 degrees square and will resolve approximately 3 arc minutes per TV line pair. Covering the surrounding display area, the Instantaneous Field of View (IFOV) fills a 125-degree horizontal by 110-degree vertical viewing volume. The resolution of the larger display changes across the field, but the average is approximately 15 arc minutes per line pair. In order to smooth the abrupt transition from one display into the other, the two displays are blended with each other in a 5-degree blend region within the border of the Area of Interest (AOI) display. Blending of the displays is accomplished by gradually reducing or increasing the brightness of the AOI within the blend region, and simultaneously increasing or reducing the brightness of the IFOV. In this way, equal luminance is obtained throughout the blend region as one display gradually fades into another. Further, the blending should reduce or eliminate any visual artifacts caused by low detail, low resolution data base models changing into high detail, high resolution data base models when the transition is made between the IFOV and AOI.

The pilot's head and eye positions are determined by lightweight helmet mounted head and eye trackers. A fixed emitter, helmet mounted sensor system determines azimuth, pitch and roll of the pilot's head with respect to the simulator cockpit. An invisible, infrared light source illuminates the pilot eye. His vertical and horizontal eye position is determined by imaging the reflected infrared light from his eyeball onto the face of a helmet mounted, infrared sensitive detector. The digital outputs from both trackers are vectorially combined in order to form the cockpit referenced pilot viewing direction. This viewing direction is combined with the instantaneous attitude and position of the simulator aircraft within the data base to arrive at a data base (ground) referenced pilot line of sight for which the image generator creates a visual display.

SECTION II

THE HELMET MOUNTED DISPLAY FEASIBILITY MODEL, SYSTEM OVERVIEW

In order to investigate the technological areas of risk, and, to a somewhat lesser extent, determine the psychophysical requirements for the proposed Visual Display Research Tool (VDRT), a small helmet mounted display feasibility model was designed and built in-house.

The feasibility model, known in-house as the Helmet Mounted Display or HMD, was not as elaborate as the previously described VDRT. Instead of two full color head and eye tracked displays, the HMD produced only a single monochromatic head tracked display. Like the proposed VDRT, the HMD was a laser scanned, helmet mounted visual display system.

An artist's sketch of the completed feasibility model is shown in Figure 2. A six-watt water-cooled argon laser provides a green laser beam which is intensity modulated by an acousto optic modulator (AOM). The video information used to drive the modulator is produced by one channel of a dual channel computer image generator (CIG) which derives its information from an appropriate data base. The video modulated laser beam is collected,

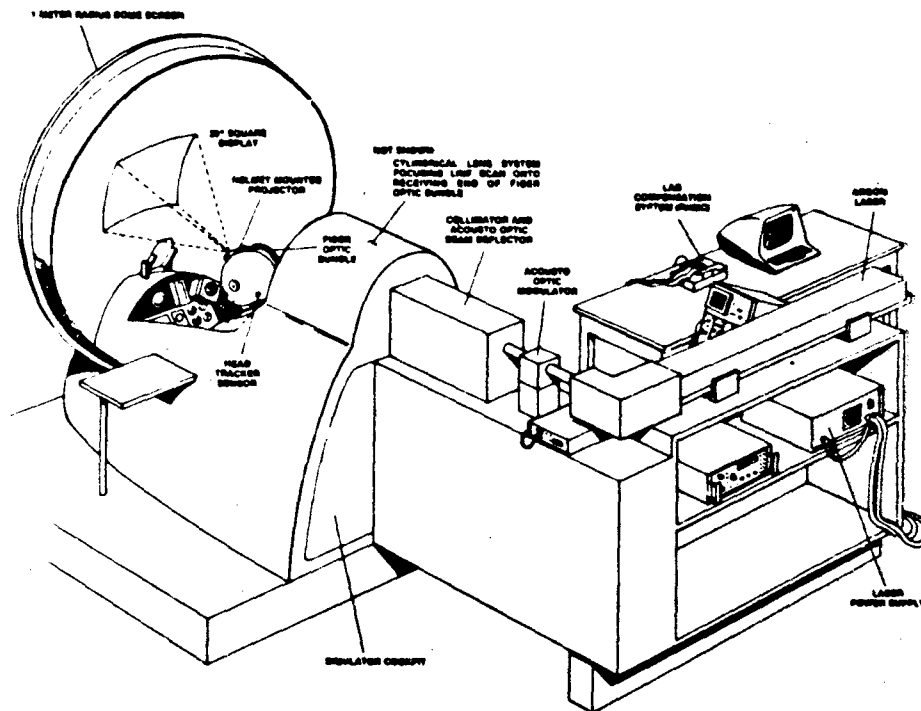


Figure 2. Helmet Mounted Display Feasibility Model.

collimated and shaped by a lens system so that it fills the aperture of an acousto optic beam deflector (AOBD). Here, the horizontal line scans which eventually form the displayed video raster are formed. The video modulated, horizontally scanned beam is again collected and focused by another series of lens elements onto one polished end of a coherent fiber optic ribbon bundle. The opposite end of the flexible two meter bundle is attached to the observer's helmet. Emerging from the helmet end of the fiber optic bundle, the line scan is projected towards a helmet mounted scanning goniometer mirror which optically deflects the line scan onto the retro reflective interior of the surrounding dome screen. As it moves, the scanning mirror sweeps the fully formed horizontal laser line scans downward on the screen, completing the displayed video raster.

Head pointing direction (HPD) is provided by a helmet mounted sensor, cockpit mounted emitter system. Electromagnetic fields radiated by the emitter are coupled into the sensor and by processing the signals obtained from the sensor, head orientation is determined.

Since flight dynamics are not included, and the cockpit controls are inactive, no simulation of an actual aircraft is possible; however, a simple joystick allows the viewer wearing the helmet to change his relative coordinates and attitude within the visual data base. The subject, then, does have control over the cockpit location and attitude within the simulated visual environment.

Before the image generator creates the display, the line of sight of the cockpit seated observer is determined. Both head pointing direction and joystick position are sampled at a 60 Hertz rate and are vectorially combined by the computer image generator in order to determine the instantaneous line of sight that the display will be created for.

Production of the video imagery filling the viewer's display requires a certain amount of processing time. The displayed video raster consists of a single video frame which is composed of two interlaced video fields. A single video field requires approximately 67 milliseconds of processing time, 16.7 milliseconds of which are for scanning and display. The video fields are produced one after the other at a 60 Hertz rate, but delayed by the 67 milliseconds processing time. To combat this induced image generator lag, a compensation system was designed and fabricated to place the viewed display along the old line of sight it was created for rather than projecting it at the observer's current line of sight.

The viewer wearing the Helmet Mounted Display sees a square video display which always remains in a forward viewing position regardless of head position. The contents of the display are updated according to where the viewer is looking and what commands the joystick is given. The appearance is much like a green tinted window that is free to move about in response to head movement.

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This system is not optimal. Certain components have been judged to be unacceptable for the final system. Some approaches which initially appeared feasible proved to be cumbersome but remained in the helmet mounted display feasibility model only for the sake of system continuity. A more critical detailed examination of the system follows in the next section.

SECTION III

FEASIBILITY MODEL SYSTEM DESCRIPTION

In this section, the major systems involved, their basic components, and their inter-relationships will be addressed.

IMAGE GENERATOR

The completed feasibility model utilizes a General Electric Compuscene Computer Image Generator (CIG) which was made available from NAVTRAEQUIPCEN's Visual Technology Research Simulator (VTRS) facility. The CIG provides a real-time video image of a digitally stored environmental data base to the helmet mounted laser projector.

The Helmet Mounted Display Feasibility Model relies upon the CIG to create the visual simulation contained within the display. The CIG provides the visual imagery that is updated at a 60 Hertz video field rate to reflect changes in the observer's head pointing direction (HPD) within the cockpit as well as changes in the simulated cockpit attitude and location within the environmental data base. In the Helmet Mounted Display (HMD), the visual display is not in a fixed location with respect to the simulator cockpit. If it were, the image contained within the display would be a direct result of the movement of the joystick by the observer. Instead, the head tracked visual scene is projected in the direction the pilot-observer happens to be looking and is updated according to both head and cockpit/joystick movement.

All of the visual scenery displayed by the HMD is the end result of processing the information contained within an environmental data base. In general, environmental data bases are composed of a number of two- and three-dimensional objects or models depicting, in a mathematical fashion, ground and cultural features. It is sufficient for the purposes of this report to consider a model to be composed of a number of flat polygons called faces. The perimeter of each polygon is composed of a number of short line segments which are joined at several points called verticies. A model is defined by the location of its verticies within the data base; the more complex a model is, the greater the number of faces and vertices it contains. In addition, each face is assigned three values representing the amounts of red, green and blue comprising its color and brightness.

The data base contains two types of coordinate systems, fixed and moving. The fixed coordinate system serves as the reference system and uniquely locates every object within the data base. A moving coordinate system is also referenced to the fixed system, but is assigned to the pilot-observer's joystick. By manipulation of the joystick, the observer is actually altering the position and orientation of a moving coordinate system within the environmental data base.

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As an observer moves his head, he changes his head pointing direction which is provided by the head tracking system. Equivalently, he is altering the orientation of a vector within the moving coordinate system. For ease in visualization, we can refer to this vector as the observer's line of sight.

Each television raster field output by the image generator requires three processing cycles. Running at a 60 Hertz update rate, each cycle requires approximately a field time or 16.7 milliseconds for completion. The cycles operate simultaneously on sequential television fields, outputting them at a 60 Hertz rate one after another in a pipeline fashion. Due to timing constraints between the first and second processing cycles, however, the pipeline process actually requires 4 field times or 66.7 milliseconds.

During the first cycle, the CIG retrieves the head tracker and joystick data, processes it, and determines the observer's position and line of sight. Visual fading factors derived from this data, fog and other environmental effects, are also determined.³ The data is not ready until 5 milliseconds into the next cycle, so it is held over one additional cycle until the start of the next full second cycle.

In the second cycle, position and line of sight data are utilized to determine the objects that are visible within the data base. Priorities are resolved (which object obscures which), and the vertices of the visual models are mapped onto a two-dimensional display plane which lies normal to the observer's line of sight. The size of the display plane or view window is determined by the physical size of the helmet mounted laser display - about 20 degrees square. Its rotation about the observer's line of sight is a consequence of head rotation. In addition, the second cycle computes sun angle, face shading and color. The data mapped onto the plane will eventually form the visual display.⁴

The third cycle completes the transformation from digital data to video. It receives a block of data in a raster line format indicating edges of faces, location, priority and color. Using the fading information and the data contained within the block, it generates one video field corresponding to the observer's field of view along his line of sight.⁵

3. Morland, D. V. and Michler, F. A. System Description, Aviation Wide Angle Visual System (AWAVS) Computer Image Generator (CIG) Visual System, General Electric Company, Space Division, Daytona Beach, FL 32015. Technical Report NAVTRAEQUIPCEN 76-C0048-1, Rev. May 1981, pp. 44-50.

4. *ibid.*, pp. 50-57.

5. *ibid.*, pp. 57-67.

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Figure 3 depicts the whole process in a timing sequence. During the first television field "0" the head tracker generates head pointing direction data, and along with the joystick data, it is transferred to the CIG for the start of cycle one processing during field "1". During field "2" the data generated by cycle one processing is buffered until the start of the next fullfield, field "3." Cycle two processing starts in field "3." The data block generated during field "3" is used during field "4" by the third processing cycle to output the video to the helmet mounted laser projector.

It is essential to understand that a video image being generated by the CIG is not displayed until 4 fields or 66.7 milliseconds after the point in time it was generated for. In essence, the image "lags" the point in time that the observer's line of sight and data base location were sampled. Without lag compensation for the image delay, the viewer will never see a correct display, and the illusion of flying through a scene with joystick control over position and attitude is lost.

Real aircraft dynamics are not included in this developmental system, instead, the joystick is used to represent movement of the observer's "aircraft" through the data base. Viewer HPD is provided by the Polhemus head tracking device, for which special hardware interfaces were designed and built to handle the data flow from the head tracker to the CIG. These interfaces provide the conversion and buffering of the data as required by the CIG data format and program timing.

LASER VIDEO PROJECTOR

Video imagery provided by the CIG is displayed by a laser video projector designed and constructed in-house. The system projects a 20 by 20 degree monochromatic TV raster display from a projector, mounted on a military flight helmet worn by the observer, onto the interior of a one meter radius dome. A beaded retro-reflective material covers the interior of the dome and provides high screen gains in the direction of the observer. The system is designed to operate at a 60 Hertz field rate, with the line rate adjustable for CIG video rates of 525 to 1023 lines per frame.

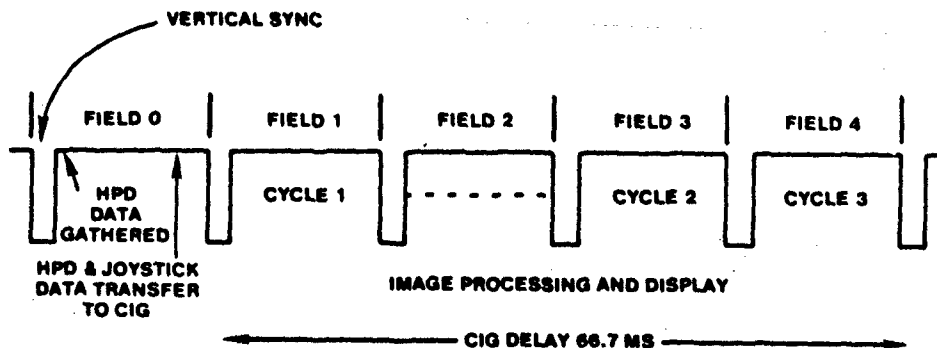


Figure 3. Processing Sequence for a CIG Display.

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Figure 4 is a block diagram of the laser video projector. The major components of the projection system are as follows:

Argon Laser
Acousto-Optic Modulator (AOM)
Acousto-Optic Beam Deflector (AOBD)
Coherent Fiber Optic Bundle
Mirror Galvanometer Frame Scanner

Each one of these system components is discussed below.

The argon laser, a Control Laser Corporation model number 553, is operated in a monochromatic mode through the use of a Littrow prism as the rear cavity mirror, yielding a single green wavelength of 5145 angstroms. The laser beam has a diameter of 1.6 mm. and a divergence of 0.4 milliradians.

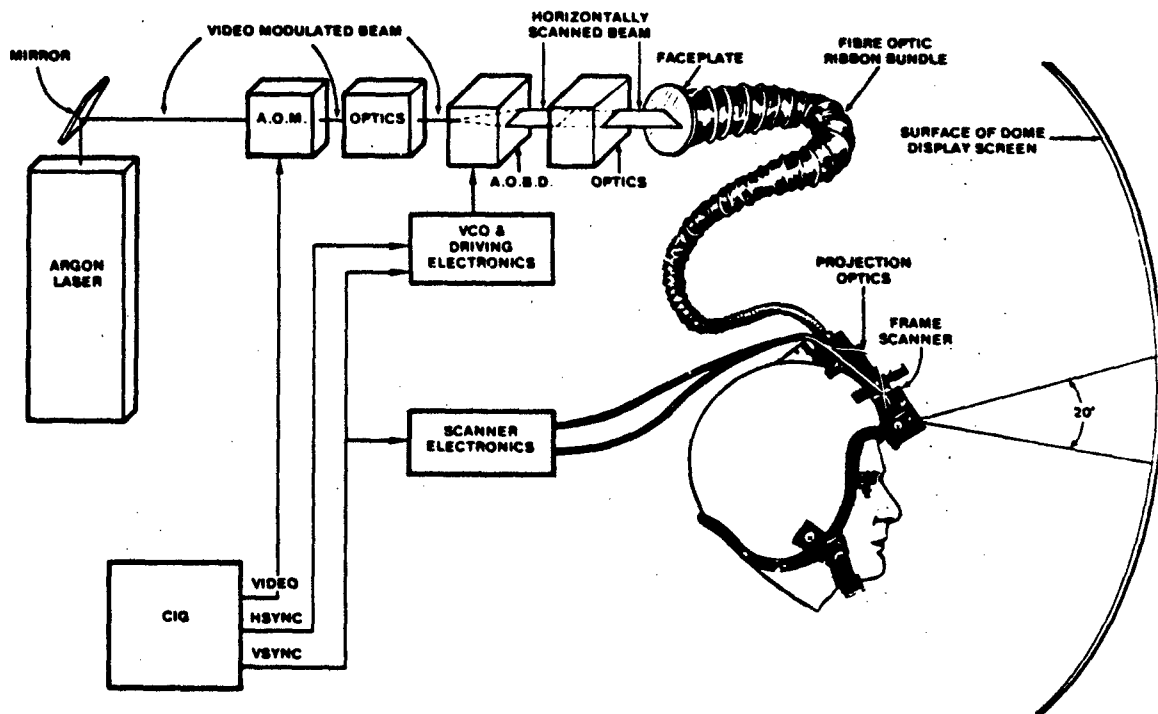


Figure 4. Block Diagram of Laser Video Projector.

The output of the laser is intensity modulated with video information from the image generator by an acousto-optic modulator, manufactured by the Intra-Action Corporation (model number 125).⁶

The video modulated laser beam is expanded by the use of a Tropel Beam Expander to a 22 mm. diameter collimated beam, and then compressed to a 22 mm. line by a cylindrical lens. This 22 mm. line is focused into the crystal of the acousto-optic beam deflector system, which deflects the first order diffracted beam through an angle of 30.6 milliradians, creating the video line scan.⁷ The deflection of the beam is controlled by a 275 - 475 MHz frequency chirp centered at 375 MHz. The chirp, or frequency sweep, is provided by a voltage controlled oscillator (VCO) manufactured by Radio Development Laboratories. A voltage ramp controls the range of the frequency sweep, its linearity, and the time required to run a full sweep. Since the horizontal video line rate varies from 1023 to 525 lines per frame depending upon the resolution of the display, the period of the voltage ramp is variable from 25.6 to 63.5 microseconds.

The AOB D was manufactured by the Harris Corporation and is made of tellurium dioxide (TeO₂). Its maximum throughput efficiency of only 15 percent places a limitation on the brightness of the final display. In addition, in order to achieve a linearly deflected, focused beam from the AOB D, it must be driven by a linearly incremented frequency sweep.⁸ In order to avoid unintentional modulation of the laser line scan by the AOB D, the output power of the voltage controlled oscillator must remain constant throughout the duration of the sweep. At the sweep rates required, the in-house designed driver for the AOB D is neither uniform in power, nor does it provide a linear sweep (the linearity required is about .01 percent). The end result is a severe loss of resolution, vertical intensity banding, and distortion in the final projected display. In Figure 5 these effects can be seen, with distortion appearing as a slight "S" shape in the normally flat runway.

After the AOB D, the beam is recollimated by the use of a second cylindrical lens to reform the 22 mm. diameter beam. A focusing lens is then used to focus the beam down to an approximate 20 micron spot size, which, due to the scanning effect of the AOB D, results in a 10 mm. wide line scan.⁹

6. Maldonado, E. D. Helmet Mounted Display Feasibility Model, Optical Design. Technical Report NAVTRAEQUIPCEN IH-340, July 1982, pp. 6-8.

7. *ibid.*, pp. 9-15.

8. *ibid.*

9. *ibid.*, p. 16.

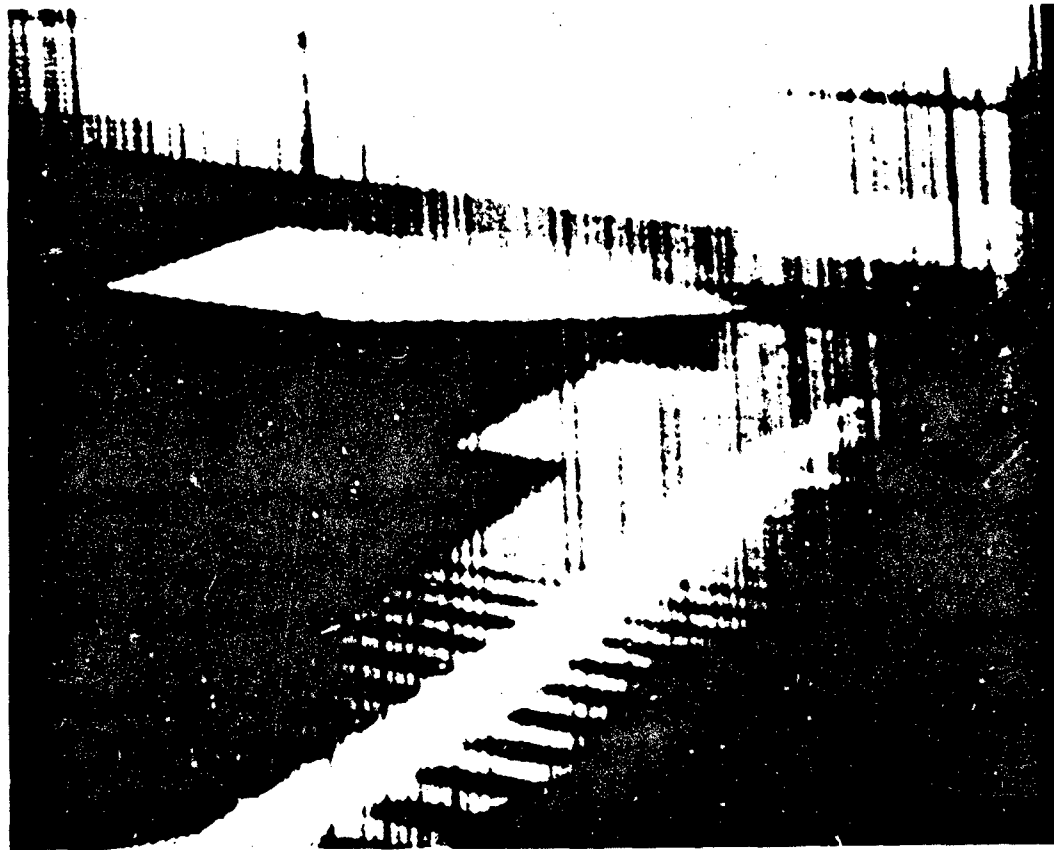


Figure 5. Displayed TV Raster as Viewed From Cockpit.

This line scan is arranged to fall on the polished faceplate of either a full frame fiber optic bundle or a flat ribbon fiber optic bundle depending upon the particular setup in use. Both coherent bundles serve the same purpose, which is to optically transport the laser line scan to the observer's helmet. The full frame coherent fiber optic bundle is manufactured by the American Optical Company. The bundle consists of individual 10 micron fibers drawn in 5 by 5 arrays which are then arranged into a rectangular grouping with dimensions of 10 mm. by 8 mm. on the faceplates. Each fiber is one meter long and has a numerical aperture of 0.56. Transmission through the bundle is limited to approximately 45 percent and mobility of the helmet mounted projector is somewhat restricted due to the stiffness of the bundle. A flat coherent fiber optic ribbon manufactured by Galileo Electrooptics Corporation is also being used. A number of 6 by 6 arrays of 10 micron fibers are arranged in a 2-meter long ribbon that is 12 fibers thick and 1002 fibers wide. The numerical aperture is .68. Mobility is much improved over the previously described "full frame bundle," although the irregularity of the fiber spacing and the number of broken fibers further reduces the resolution, and places dark vertical stripes on the display (see Figure 5.)

The second face of the fiber bundle is mounted to the helmet and arranged to lie in the focal plane of a 15 mm. projection lens. After the projection lens, the laser line scan encounters a closed loop, moving iron galvanometer mirror scanner obtained from General Scanning, Inc. (model number 100PD). Servo controlled by a General Scanning controller (model number CCX-102), and driven by the 60 Hertz vertical sync from the CIG, the scanner mirror deflects/sweeps the laser scan lines vertically as they are projected onto the interior surface of the dome screen, providing the vertical scanning required to form the completed TV raster previously referred to in Figure 5.¹⁰

HEAD TRACKER

The head tracker, a SHMS III-A procured from Polhemus Navigation Sciences, Inc., computes the observer's head pointing direction with respect to the simulator cockpit. Known in-house as the Polhemus head tracker or "PHT," the basic system consists of a magnetic field radiator, a magnetic field sensor and a controller - the electronic systems unit. Mounted on the observer's helmet, the small, lightweight sensor moves within a magnetic field generated by the cockpit mounted radiator. As the orientation and position of the helmet mounted sensor changes, the magnetic field coupling between the emitter and sensor also changes.

The sensor as well as the radiator each consist of three small orthogonal coils. Excited sequentially by a 10.6 kHz. frequency burst, the radiator produces three magnetic fields whose axes are orthogonal to each other. Each orthogonal radiator coil emits a magnetic field for a small period of time and, during the time the field is active, each one of the sensor coils is sampled.

The field generated by the active radiator coil is symmetrical about an axis that coincides with the axis of the radiator coil. The orientation and position of each sensor coil within the generated field determines the amount of current induced to flow in the sensor coil. By performing a mathematical operation upon the signals obtained from the three sensor coils, the sensor's orientation relative to the axis of the emitting field can be determined. Its position relative to the axis is not yet fully determined due to the symmetry of the field about the axis. This operation is performed three times, once for each field generated. When the above operation has been performed for each of the three radiated fields, the position and orientation of the sensor relative to a three axis coordinate system can be determined.

The sequence which determines the position and orientation of the sensor relative to the radiator is an iterative process which is initiated by the vertical sync signal once every 16.7 ms. Figure 6 depicts the process in a general fashion.

10. *ibid.*, p. 18.

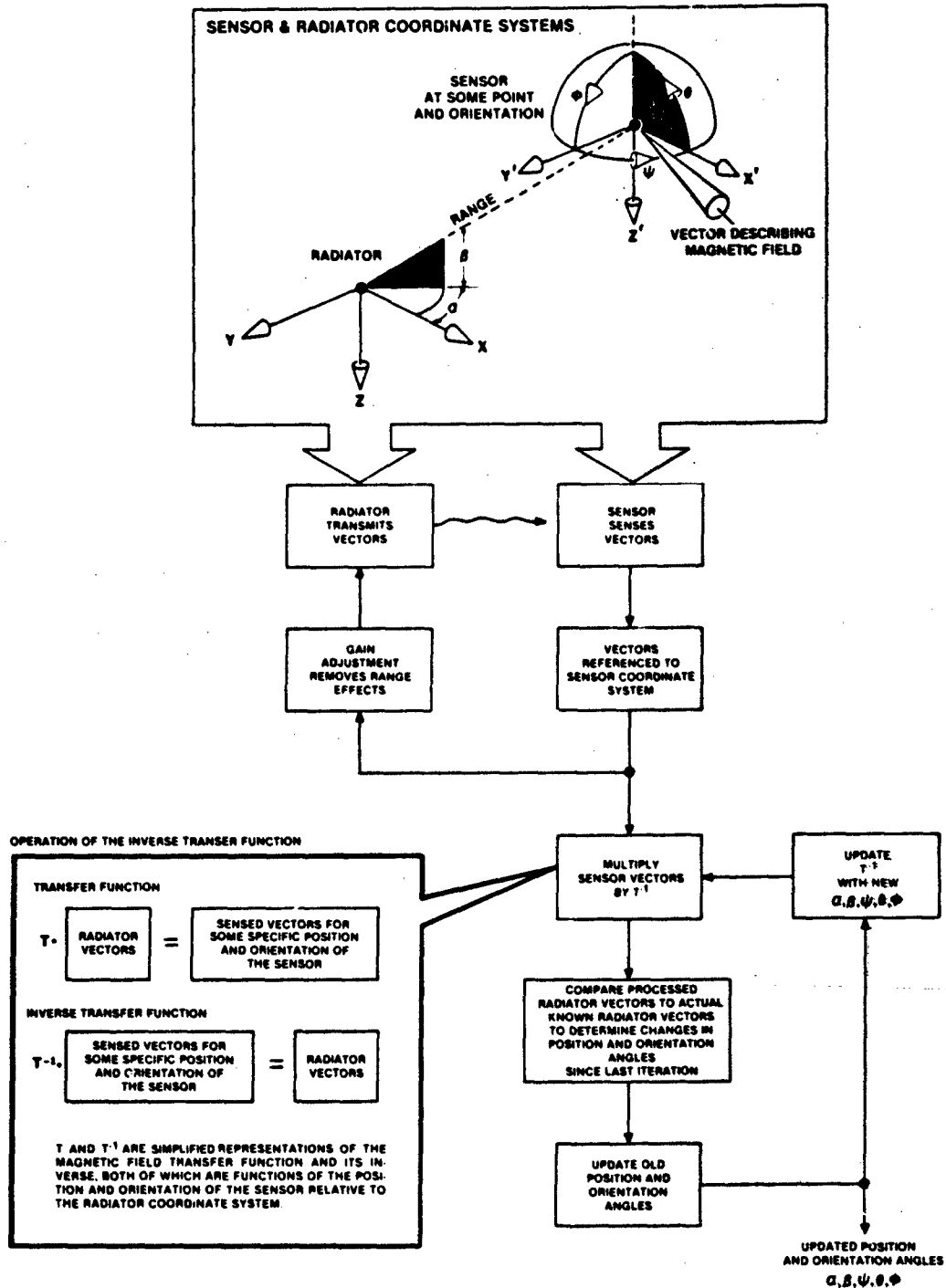


Figure 6. Basic SHMS III-A Processing

The magnetic field generated by a radiator (coil oriented along the "X" axis (the observer's forward axis) for instance, can be described at some arbitrary point as a vector referenced to the radiator coordinate system. The sensor, which happens to be located at that point, will have different currents induced in its coils by the field. These currents will describe the vector in terms of the sensor coordinate system. Each time a radiator coil becomes active and generates a field, it is described by the sensor coordinate system, arbitrarily located at some point within the field, as a vector. After the three fields have been emitted sequentially, and described in terms of three vectors referenced to the sensor coordinate system, they are operated upon by an inverse magnetic field transfer function.

For simplicity, the inverse transfer function will not be described in any great detail. Instead, it will be described as a mathematical operation that is a function of sensor position (alpha and beta) and orientation (psi-azimuth, theta-pitch, and phi-roll) with reference to the radiator coordinate system. For a given current, driving a radiator coil with some fixed dimension and number of turns, there is an associated magnetic field. This field can be fully described, using a suitable coordinate system, as a vector at any point distant from the coil. In a like manner, the three orthogonal fields generated by the radiator are also fully describable at any point with reference to the radiator coordinate system. Suppose a second moving coordinate system, the sensor coordinate system, is introduced. As long as its orientation and position with respect to the fixed radiator coordinate system is known, the field vector can also be described in terms of the moving sensor coordinate system. Figure 6 depicts a mathematical operation on the vector which is in terms of the radiator coordinate system. The output of this operation is the vector in terms of the sensor coordinate system. The operator is the transfer function "T" which is a function of position and orientation of the sensor with respect to the radiator. If the output of the previous operation is operated upon by the inverse transfer function, "T-1", the result is the vector with respect to the radiator once again. In effect, the inverse transfer function has undone the previous operation.¹¹

Looking at Figure 6 once again with particular attention to the processing sequence, the vectors as referenced to the sensor are multiplied by the last known correct inverse transfer function, using the last known alpha, beta, psi, theta, and phi. The output of the operation, if the position and orientation are correct, is the characteristic field known to be emitted by the radiator. If the last alpha, beta, psi, theta and phi are incorrect, the outputs are not the correct field vectors with respect to the radiator, and the difference is linearly related to the true alpha, beta, psi, theta and

11. Anon. Operation and Maintenance Manual for the SHMS III-A, SPASYN Helmet Mounted Sight, Polhemus Navigation Sciences, Inc., Post Office Box 298, Essex Junction, VT 05452. November 1980, OMN-1024-1, pp. 4:1-4:18.

phi. The new position and orientation angles are computed and output, and the inverse transfer function is updated for the next iteration. Range is determined by adjusting the current to the radiator coils and/or sensor gain in such a manner that the vector measured by the sensor always has some constant length. A more rigorous treatment of the processing sequence may be found in Reference 12.

In the HMD system, the sensor is mounted on the helmet and the radiator placed immediately behind the cockpit seat. Hence, sensor orientation is analogous to head orientation or more concisely, HPD.

As previously described in the section entitled "Image Generator" (page 12), the cockpit referenced HPD is used by the CIG to compute the observer's line of sight. Although both position and orientation of the sensor are provided by the SHMS IIIA, only the sensor orientation is used to determine the observer's line of sight. Strictly interpreted, this simplification is not mathematically correct. It is simply expedient, since in the case of the feasibility model, the extreme range at which objects within the data base are typically viewed precludes the visual effects of minor head translation.

Because the head tracking system relies upon magnetic field coupling, there are limits to the extent of the radiator/sensor separation. This is referred to in Polhemus literature as the "motion box." The range extends 16 inches forward of the radiator (X direction), plus or minus 8 inches from side to side (Y direction) and 8 inches downward from the radiator (Z direction). Operation outside these limits results in performance degradation. When the head tracker is installed in the Helmet Mounted Display Feasibility Model, the following performance specifications are met:

STATIC ANGULAR ACCURACY
plus or minus .5 degrees at 50 percent CEP
(50 percent of the time, the output is within
+/- .5 degrees)

ANGULAR JITTER
1/10 degrees peak to peak (roughly
equivalent to 1 bit out of 12 bits)

12. Raab, Fredrick H.; Blood, Ernest B.; Steiner, Terry O.; and Jones, Herbert R. Magnetic Position and Orientation Tracking System, in IEEE Transactions on Aerospace and Electronic Systems, Vol. AES-15 No. 5, September 1979, pp. 709-718.

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UPDATE RATE

synchronized to CIG 60 Hertz video field rate (SHMS IIIA can free run at faster rates, however, cycle time is irregular)

DYNAMIC ANGULAR ACCURACY

for normal head rates (600 degrees per sec or less) essentially defined by the number of degrees that the head moves during the 16.7 ms. required to compute HPD.

Formatted serially, the digital data consists of six 17-bit words output in the following order: yaw, pitch, roll, X (forward direction from the radiator) Y (lateral movement), and Z (vertical motion). The first 12 bits of each 17-bit word are significant data, the next 4 are noise, and the last bit is a parity bit. The hexadecimal values for the rotational data are as follows:

	HEX VALUE		
	C000Hex	8000Hex	4000Hex
Yaw	Right 90 degrees	Center	Left 90 degrees
Pitch	Up 90 degrees	Center	Down 90 degrees
Roll	Right 90 degrees	Center	Left 90 degrees

About 14 to 15.5 ms. after the initial sampling procedure, the SHMS III-A provides a "data ready" pulse. This is a signal to the interfacing hardware that the processing is complete, and the head pointing direction (HPD) data is available. In the current configuration, the in-house designed interfacing hardware clocks out the data before the beginning of the next sync pulse (vertical sync) which occurs every 16.7 milliseconds (see Appendix). This sync pulse starts a new HPD data gathering cycle. During operation, the head tracker delivers HPD data at a 60 Hertz rate with a delay of approximately one field time between the sampled HPD and the HPD data output.

IMAGE LAG COMPENSATOR

During the development of the feasibility model, the problem of scene instability quickly became apparent. Without compensation, due to the time required for head tracker and CIG computations, there exists an error in image placement during head motions. Since the problem is especially apparent during a rapid head movement by the observer/pilot wearing the helmet mounted projector, the solution to this problem came to be known as Rapid Head Motion Compensation (RHMC). The compensation mechanism involves the use of a micro-processor with software that controls the relative projection angle of the imagery from the viewer's helmet in response to image displacement error. Change in the image projection direction is accomplished via offsets input into the vertical and horizontal sweep of the laser video projector. In this section, an examination of the cause, effects, and the solution devised for scene instability will be discussed.

The problems that arise from rapid head motions are due to the discrete sampling of the head pointing directions and the finite time involved in providing an updated image via the CIG. This results in an image placement error coinciding with head motion and is manifested in an apparent motion of what should be stationary objects in the subject's FOV. With no compensation, objects appear to "swim" during the start and finish of a head motion and are displaced during the actual head motion.

Consider the viewer to be at some stationary position within the data base. Further, consider the head of the viewer to be stationary with an image projected onto the screen from the HMD. Objects within the displayed image are stable as long as the viewer does not move his head because the displayed image is being computed and displayed for a fixed line of sight. Returning to Figure 3, when the viewer changes his head pointing direction (HPD), at the start of field "0," the head tracker doesn't compute a new HPD until just before the next vertical sync. This new set of yaw, pitch, and roll data reflects the HPD of the viewer at the sampling time, not at the time of the HPD output. The time between the sampling and output of the HPD data, one field time or 16.7 ms., is one source of delay in updating the image. Another source of delay in updating the image after the occurrence of a head motion is the time required for the CIG to take in new head pointing data and then to compute an image based on the new viewer line of sight. As previously described in the "Image Generator" section, the CIG requires 4 fields to generate and display the image.

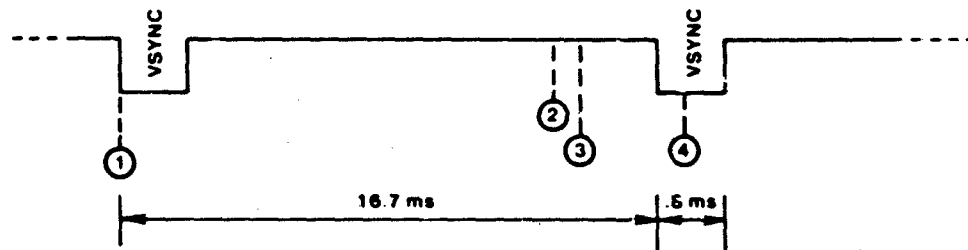
If the viewer has moved his head during the five field times that occur between HPD sample time and the display of the image based on that sample, he will observe an incorrectly displayed image. A 5 field, or 83.5 ms., time lag exists between the old line of sight the image is created for and the current line of sight the image is being projected towards.

To visualize the effects of the 83.5 ms. time lag, suppose that the projected image contains a tree as an object in the center of the display. Without compensation, a head motion to the right of 2 degrees during the above time interim between sampling and display will result in the tree also moving 2 degrees to the right. All objects in the image will retain the same orientation they had before the head motion and the scene will be incorrectly displayed until the process of computing a new HPD and subsequent CIG image display for the new line of sight is completed. When the viewer completes the head motion, the tree will at that moment be displaced to the right followed by a gradual movement of the tree to the left as the CIG generates the correct image for that particular line of sight. Obviously, this effect can be very disorienting to the viewer, for trees should be rooted in the ground and stationary. Not only objectionable from a subjective standpoint, it is highly probable that an improperly placed image can result in negative training cues to the prospective trainee. As a consequence, it is desirable that the image lag be reduced to some tolerable level.

The Rapid Head Motion Compensation System reduces the previously described image delay problem. Essentially the hardware, under software control, moves the raster in such a manner as to keep objects in the FOV from moving as the pilot changes his HPD. The RHMC system performs compensation based on the current HPD sample compared with the HPD that was used to compute the image to be displayed next. The difference between these HPDs is massaged by software and sent to raster shifting hardware to shift the projected imagery horizontally and vertically opposite the direction of head motion. The system attempts to place the display physically along the old line of sight it was created for.

For the HMD feasibility model, the angular error in line of sight amounts to the movement of the viewer's head over five video field times. The software that corrects this error has been named "5THPREV," referring to the number of video fields delay involved. The software is written in 8085 assembly language and is designed to provide raster shift values within the timing restraints shown in Figure 7 (see Appendix A for flowcharts and additional detail). This timing diagram shows the initialization of the PHT data gathering and calculation cycle by the vertical sync of the video, followed by a "data ready" some 15 milliseconds later. The software then takes the HPD from the PHT data controller (see Appendix A) and, after processing, outputs the raster shift values before the next vertical sync. In general, the program is configured to allow compensation for any number of "fields" delay (depending on the specific CIG delay) and is referred to as "NTHPREV."

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- ① → ② PHT PERFORMS MEASUREMENT AND CALCULATION PROCESS. (15.5 ms)
- ② → ③ H.P.D. DATA IS READY AND ACCEPTED BY 8085.
- ③ → ④ SHIFTING VALUES ARE CALCULATED. OUTPUT OCCURS AT ④
- ④ → ② STORAGE TABLES ARE SHIFTED 8085 WAITS FOR PHT DATA READY.

Figure 7. RHMC Timing Diagram.

A graphical illustration of the effects of compensation on the display is provided by the graphs in Figure 8. Consider the simulator cockpit to be fixed at some point within the environmental data base used to create the visual display and for simplicity, consider all angular motion relative to the simulator cockpit. In the first graph, an arbitrary horizontal head movement by a viewer wearing the helmet mounted projector is followed one field later by the head tracker output. Three fields after the head pointing direction (HPD) data is made available, the CIG completes the processing, and during the fourth field, the generated image is displayed. Since the projector is physically attached to the observer's head, the projector heading (i.e., its projection axis) is identical to the viewer's head pointing direction. In the graph the first curve to the left represents actual head motion, the second curve, the PHT output, and the third curve, the angular heading for which the image being displayed was calculated. The vertical separation between the viewer head motion curve and the CIG image heading curve represents the uncompensated angular image lag, which the viewer observes as an incorrectly positioned image. As previously mentioned, the image lag is equivalent to the angular distance traveled by the head during five TV fields or 83.5 milliseconds.

The second graph in Figure 8 depicts the operation of the rapid head motion compensation system. It can be understood as follows: since the image lag amounts to five fields of head travel, the heading of the helmet mounted projector needs to be shifted back five fields of head travel in order to

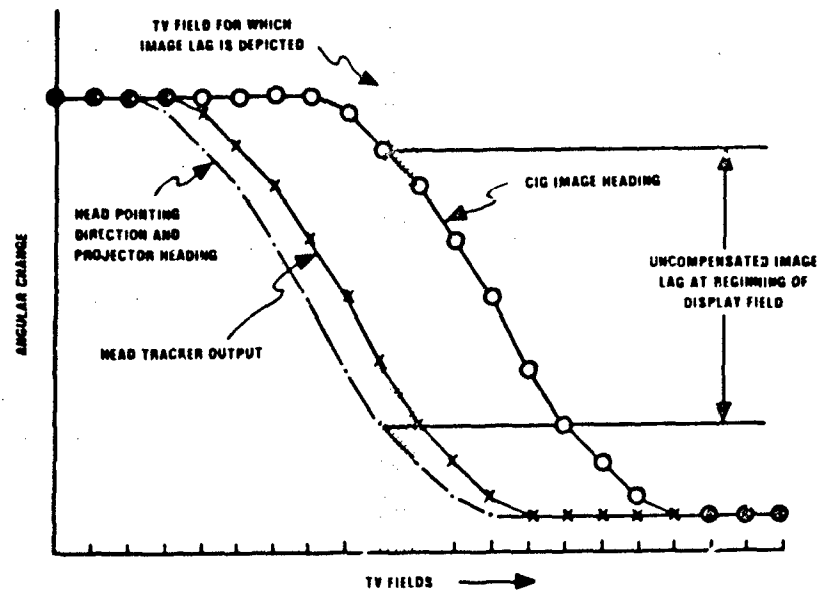


FIGURE 8A

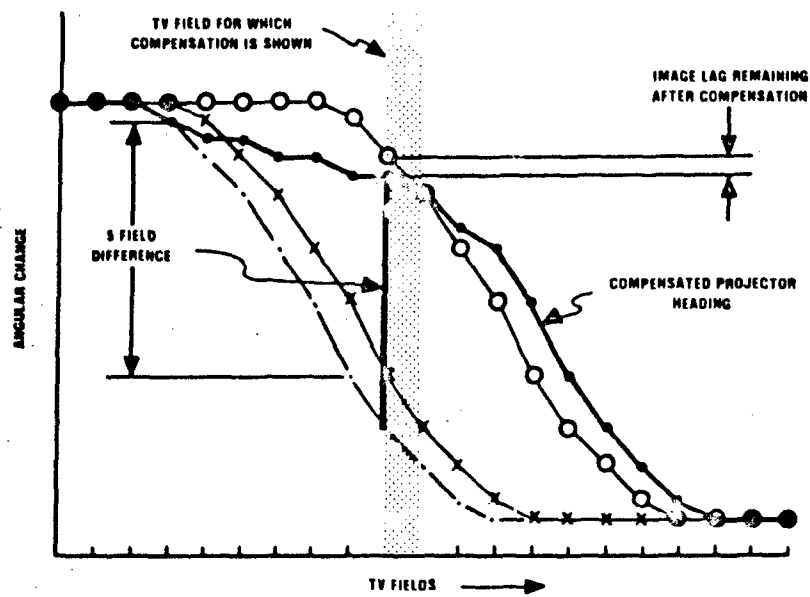


FIGURE 8B

Figure 8. Effects of Lag Compensation.

coincide with the heading of the displayed image. The projector heading is changed by offsetting the position of the horizontal line scan. The offset is performed during the vertical blanking interval just prior to actual display of the image. The most recent head position information available is received just before the occurrence of vertical sync. The difference between the most recent HPD data and the fifth previous piece of HPD data amounts to the angular change in head position over five fields. Essentially then, the projector heading is changed using the most recent five field head position change available. This operation is graphically illustrated by noting that the five field difference "DIFF 5" (see Appendix A, RHMC Software) is added to the actual head position at the beginning of the display field via horizontal raster shifting. This produces a compensated projector heading, where the difference between the compensated heading and the CIG image heading is angular discrepancy still remaining after compensation. Note that although the compensation is not perfect, the remaining image lag is considerably less than the uncompensated image lag, and the image is generally compensated when the viewer's head has completed the motion.

Further information detailing the implementation of both the software and the hardware in Rapid Head Motion Compensation can be found in the Appendices of this report.

SECTION IV

OBSERVATIONS AND CONCLUSIONS

It's clear that neither fiber optic bundle transmits a totally acceptable line scan. The full frame bundle, utilized because of its in-house availability, offers many redundant rows of fibers on which a line scan can be focused. Still, finding a row or group of rows which has no broken fibers is impossible. Unlike the full frame bundle, the ribbon bundle provides improved mobility, but at the expense of unevenly spaced fibers, a quantity of broken fibers and poorly polished fiber ends. Despite these contrary observations, a coherent fiber optic ribbon bundle should be available and suitable for future use with development of appropriate manufacturing techniques.

The Acousto Optic Beam Deflector (AOBD) produces an unevenly focused, non-linear horizontal line scan. This is due to the VCO's inability to supply a linear frequency chirp with a power variation of less than ± 2 db. Power variation results in a line scan that varies in brightness. Non-linearity in the chirp produces a non-linear line scan that varies in focus. Attempts were made to linearize the line scan by suitably shaping the ramp signal that served as the input to the VCO. One promising method involves the use of a fast digital to analog converter. The in-house efforts, however, met with little success. At present, the best alternative seems to involve the use of a high speed, rotating scanner mirror system manufactured by Speedring, a division of Schiller Industries, Inc., which is now planned for use in the Visual Display Research Tool.

The display distortion and lack of resolution was judged objectionable by most viewers. Display distortion was far more than the typical viewer would observe on his own home television although exact measurements were not made. Figure 9 shows a test grid as displayed by the HMD system. The distortion occurs both vertically and horizontally, although the horizontal distortion is more extreme. The resolution was determined to be approximately 200 TV line pairs under the most optimal conditions.

The head tracker utilized is acceptable for this particular visual display. Some minor modifications were made which reduce the HPD data filtering. This decreases the settling time for small angular step changes but increases the jitter in the HPD data. Since the resolution of the feasibility model's display is low, the jitter is not directly observable by a subject wearing the helmet. In order to preserve the resolution of the imagery presented by the follow-on VDRT, it has been determined that a head tracker with at least 14-bit accuracy or better is required to keep the jitter at a pixel or sub-pixel level. If the helmet mounted sensor and cockpit mounted emitter are properly placed, the aluminum housing of the projector (a moving metallic mass) does not appear to significantly affect the accuracy of the HPD data. Generally, it is felt that the absolute accuracy of the head tracker is less important than its ability to resolve small angular changes and provide low noise data rapidly.

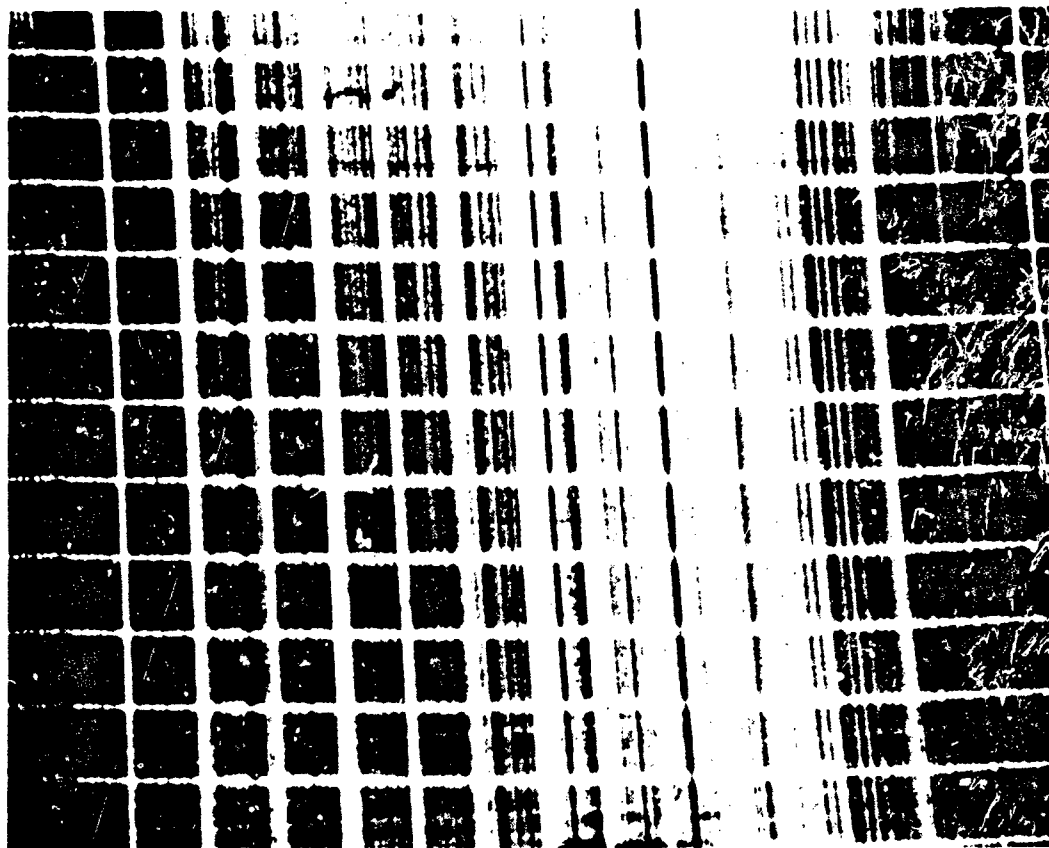


Figure 9. Grid Patterns Displayed by Helmet Mounted Projector.

The overall effect of the RHMC system is an increase in scene stability during head motions of the observer. During the testing, tweaking and evaluation of the feasibility model, many people viewed the display with RHMC both operational and non-operational. With the compensation system functioning, most indicated the image lag was not directly observable; when the compensation system was switched off, all viewers were acutely aware of the swimming effects caused by the lag. Those intimately familiar with the system could cause lag effects simply by exceeding the shifting capability of the RHMC system. Although a cause of concern at first, no compensation was provided for head roll. It seems that most viewers were incapable of achieving roll speeds at which the effects might be observable or, the display was too small to observe them. No roll compensation is planned for the VDRT.

Several major issues remain unresolved. An eye tracker will be required in the VDRT; yet, there is no known method which combines the properties of rapid update and unobtrusive measurement. Raster shifting will produce some display distortion when used in a wide FOV system (such as the VDRT). The distortion correction, if any, that may be required of the CIG remains to be determined. One additional issue concerns data base modeling. In the VDRT,

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objects within the environmental data base will consistently be making the transition from the low resolution IFOV, where they are modeled in relatively low detail, into the high resolution AOI where they become high detail models. The blend region around the AOI should reduce the problem somewhat, but unfortunately, the change in detail will take place in the motion sensitive peripheral viewing region of the eye. It is not clear at this point how to model objects within a data base to make the transition unobtrusive. Still more investigation and research is needed for answers.

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APPENDIX A

RHMC SOFTWARE

The software for RHMC has two functions. One function is to keep a record of past HPD values and then to calculate the required amount of raster shifting for proper image placement. This function is interrelated with the PHT and CIG video timing, with the vertical sync of the CIG video being the master timing signal for the software and PHT. The second function is essentially transparent to the logic flow of the software and concerns the loading of three data buffers for the transfer of HPD data to the CIG.

The software has several tasks in order to accomplish raster shifting. First is the initialization and updating of two tables in RAM for the storage of past and present HPDs. These two tables, one each for vertical and horizontal data, are shown in Figure A1. The most recent (or present) values, W-0, are placed at the top of the tables and moved down to the W-1 position when a new HPD data set is obtained. This downwards movement of an HPD value in the tables continues each time a new data set is obtained (W-1 to W-2, W-2 to W-3, W-3 to W-4, W-4 to W-5) until the data is no longer needed and is discarded. Initialization of the tables is performed by subroutine TABLESET which loads the boresight values (zero degrees) into the two tables. The downward movement of the table values is accomplished via the subroutine FIFO during the time that the PHT is calculating the new HPD values.

The length of the tables determines the number of HPD values to be stored, and at the same time, implies the number of field times delay for which the program will compensate. For a five field delay in PHT to CIG image presentation, the tables must store the five previous HPD samples plus the present sample for a total of six HPD words per table. The error in image placement, for an exact five field delay, is simply the difference between the present sample (W-0) and the W-5 sample. With the present sample always at the top of the table and the fifth previous sample always at the bottom, the error value is found by subtracting the last word in the table from the first word. Below each table there are two reserved bytes of RAM that are used to store the sign of the angular error and the value of the shift word to be sent to the output DACs for shifting the raster.

Figure A1 also shows the reserved RAM areas for a table of input values which are used to determine the length of the HTABLE and VTABLE and to set up needed constants. The values (H or V)INITIAL and (H or V)FINAL are the first and last RAM addresses used to store HPD samples (2 bytes per sample). For five fields delay and the required six sample storage, 12 bytes are needed per table. In the figure, the HINITIAL value is 2020hex and HFINAL is 202Bhex. The (H or V)SOURCE values are used by FIFO to point to the first byte to be moved two addresses downward, with the (H or V)INITIAL values indicating the last byte to be moved. Constants in the Input Table are as follows:

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INPUTS			HTABLE	
2000	20	HINITIAL	2020	HW ₀
2001	20		2021	HW ₀
2002	30	VINITIAL	2022	HW ₁
2003	20		2023	HW ₁
2004	29	HSOURCE	2024	HW ₂
2005	20		2025	HW ₂
2006	30	VSOURCE	2026	HW ₃
2007	20		2027	HW ₃
2008	2B	HFINAL	2028	HW ₄
2009	20		2029	HW ₄
200A	3B	VFINAL	202A	HW ₅
200B	20		202B	HW ₅
200C	0D	HCONTROL	202C	SIGN
200D	0D	VCONTROL	202D	HSHIFT
200E	A7	HCENTER	202E	
200F	A7	VCENTER	202F	
2010	00	HZERO		
2011	80			
2012	00	VZERO		
2013	80			
2014		MASK VALUE	2030	VW ₀
2015	3B	HMAX	2031	VW ₀
2016	3B	VMAX	2032	VW ₁
2017			2033	VW ₁
2018			2034	VW ₂
2019			2035	VW ₂
201A		SCRATCH1	2036	VW ₃
201B			2037	VW ₃
201C		SCRATCH2	2038	VW ₄
201D			2039	VW ₄
201E			203A	VW ₅
201F			203B	VW ₅
			203C	SIGN
			203D	VSHIFT
			203E	
			203F	

Figure A1. NTHPREV Reserved RAM Inputs and Tables.

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- (H or V)CONTROL - provides for the fine adjustment of shift values sent to DACs (see subroutine ADJUST).
- (H or V)CENTER - centering values for raster to be sent to the DACs.
- (H or V)ZERO - the boresight (or zero degree value) used to initialize the tables.
- MASK - value used in setting 8085 mask for interrupt priority.
- (H or V)MAX - limit the shift values sent to the DACs (must be set less than 3Bhex).

There are also four bytes reserved below the Input Table for temporary storage purposes designated as SCRATCH1 and SCRATCH2.

Once the HTABLE and VTABLE are initialized and an update is received from the PHT, the process of computing the two 8-bit words for controlling the raster placement on the target plane of the projection lens begins. This process is performed by subroutines HSHIFT and VSHIFT for the horizontal and vertical offset values. Referring to the flowchart for HSHIFT in the appendices, the first step is to find the difference, HDIFF, between the present and fifth previous horizontal samples as explained previously. The next step is to use the HDIFF value to calculate the HSHIFT offset value.

The HSHIFT value is dependent on the target plane raster size, the projections lens, and the reference voltage for the DACs. The HSHIFT value for the laser based HMD system is calculated according to the focal length of the lens and the required displacement of the raster to effect an angular shift of the projected image equal to the HDIFF value. Suppose that the HDIFF value represents a 1-degree movement of the viewer's head. This corresponds to a 16-bit value of 00B0hex (or 176decimal) for HDIFF. HDIFF must then be scaled to the proper value which will shift the raster horizontally on the target plane and result in an angular shift of the imagery being projected by 1 degree.

To find the scale factor for the horizontal channel, the 8-bit word required to displace the raster line one quarter of its length was experimentally determined to be 32hex or 50decimal. Knowing the focal length (8 mm.) at the target plane, an offset of 32hex results in a 7.6 degree shift of the projected imagery. This corresponds to a 0.15 degree shift of the image per unit offset increment sent to the horizontal digital to analog converter (HDAC). Therefore, to shift the image by 1 degree, an offset value of approximately 07hex is needed. Hence, a scale factor of 1/26 decimal is needed to scale the HDIFF value of 00B0hex to its proper value of 07hex before being sent to the HDAC. However, due to the limited instruction set of 8085 up, division by 26 is not directly accomplished. To solve this problem, the

direction taken was to add a percentage of the HDIFF value to itself (in the form of $N \cdot \text{HDIFF} / 32$ or $N \cdot 3$ percent of HDIFF) and then to divide this new adjusted HDIFF, NHDIFF, by 32 (by shifting NHDIFF 5 bits to the right) to effect an approximate division by 26. This adjustment is performed by subroutine ADJUST, which also allows minor adjustment in the RHMC shifting to account for delays which are not integer multiples of field times. After the magnitude of the horizontal offset value is found, the sign of the angular difference is used to determine whether to add or subtract the offset value to or from the raster centering value. This decision determines the shift direction to be either to the right or left depending on the direction of head motion.

The VSHIFT value, however, is not dependent on the projection lens or the raster size. This is due to the fact that the angular shifting of the image in the vertical direction is performed by offsetting the central positioning of the frame scanning mirror, which is located after the projection lens. Here, the 8-bit word required to shift the image in the vertical direction by 4 degrees was experimentally determined to be 16hex (or 22decimal), resulting in a 0.18 degree shift per unit offset sent to the VDAC. These constants indicate that the scale factor for the vertical channel should be 1/29decimal. Once again, the ADJUST subroutine allows for an effective approximate division of VDIFF by 29 and minor adjustment of the shift value magnitude. When the VOFFSET magnitude is calculated, the sign of the angular difference is used to determine whether to add or subtract the VOFFSET magnitude to or from the vertical raster centering value.

The overall effect of the RHMC system was an increase in scene stability during head motions of the observer. Once the system had been incorporated into the HMD, subjective experiments were performed to fine tune the compensation effect by varying the control words for the ADJUST subroutine. These control words were found to be valuable in adjusting for changes in the focal length of the final projection lens, as well as for their intended use of providing a means to compensate for CIG-PHT delays that are integer multiples of a field time.

Sometime just before or during the pending vertical sync, the RHMC program finishes calculating the two 8-bit words representing respectively the horizontal and vertical raster shift (HSHIFT and VSHIFT). Then the system enters a loop and waits for the next occurrence of vertical sync (7.5 interrupt); when vertical sync occurs, the program responds by outputting the two 8-bit words to the horizontal and vertical digital to analog converters (HDAC and VDAC). The voltage output of the DACs control the extent of the raster shift required. The output of the HDAC frequency shifts the chirp that drives the acousto optic beam deflector (AOBD), causing an offset of the horizontal line scan. Shifting the helmet mounted mirror scanner with the VDAC raster is done only during the vertical retrace time (i.e., during the vertical sync). By introducing a shift during the time that the video is blanked, the whole raster is shifted as a unit and tearing or separation of the displayed raster is avoided.

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ASAP80 F3 LPREV SRC DEBUG MOD85

IS15-II 8888/8885 MACRO ASSEMBLER. V3 8

LPREV

LOC OBJ LINE SOURCE STATEMENT

1 NAME LPREV

2 ,

3 ,

4 ,

5 ,

UPDATED FOR LASER PROJECTOR JULY 2 1981

6 ,

7 ,

8 ,

9 ,

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REJECT

```
*****
*                               *
*      LPREV                    *
*                               *
*****
```

THIS PROGRAM IS A MODIFICATION OF NTHPREV FOR THE LASER DISPLAY SYSTEM

NTHPREV IS THE MAIN PROGRAM FOR RAPID HEAD MOTION COMPENSATION. THE PROGRAM COMPENSATES FOR CIG DELAY TIME IN THE PHT-CIG-VIEWER LOOP. THE BASIC ALGORITHM USES THE DIFFERENCE IN HEAD AZIMUTH AND ELEVATION FROM THE PRESENT VIDEO FIELD TO THE NTHPREVIOUS FIELD. THIS DIFFERENCE IS USED TO OFFSET THE RASTER IMAGE OPPOSITE THE DIRECTION OF HEADING CHANGES (VERT. AND HORIZ. ONLY).

THIS OFFSET IS ADJUSTABLE VIA THE EQUATION

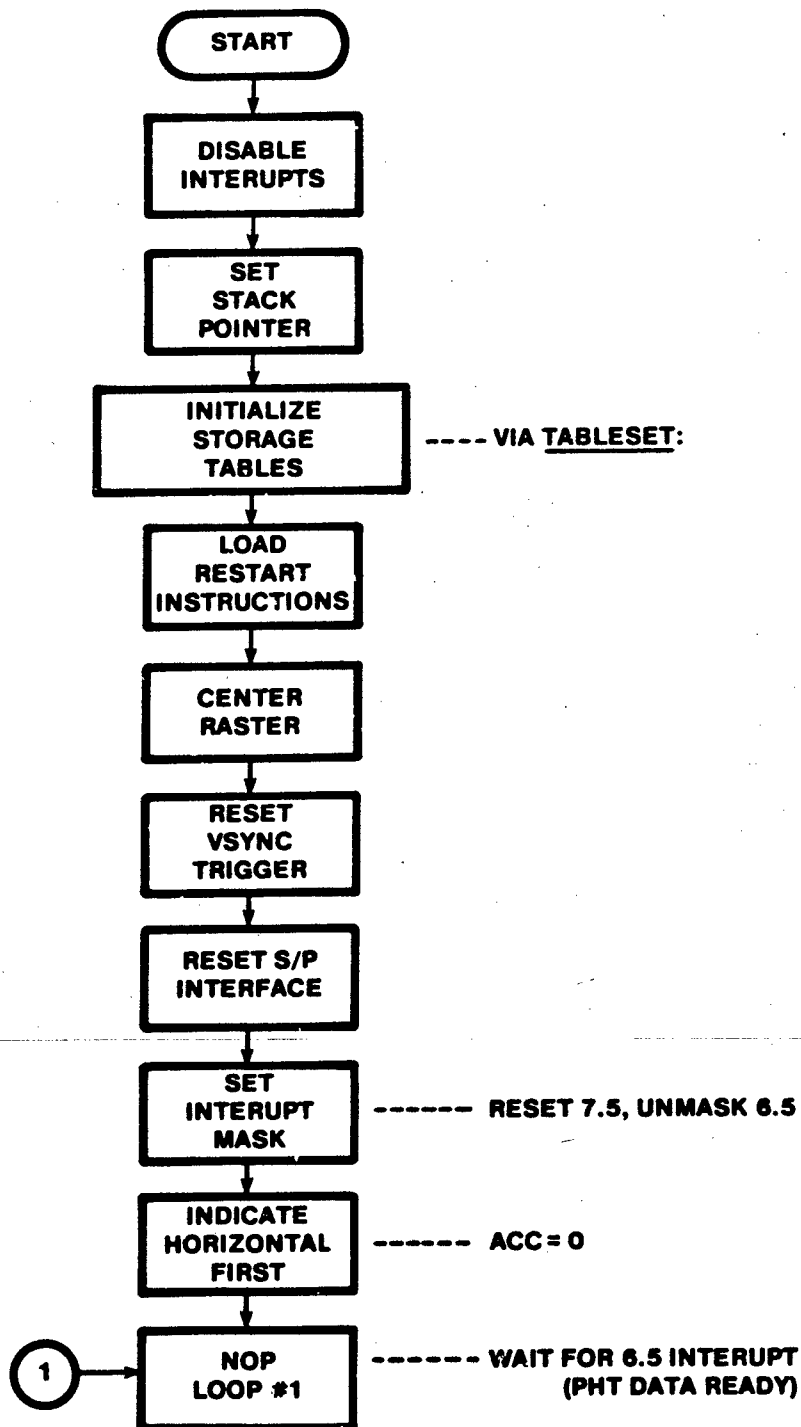
$$\text{OFFSET} = \text{DIFF} \leftarrow N * (\text{DIFF}/16)$$

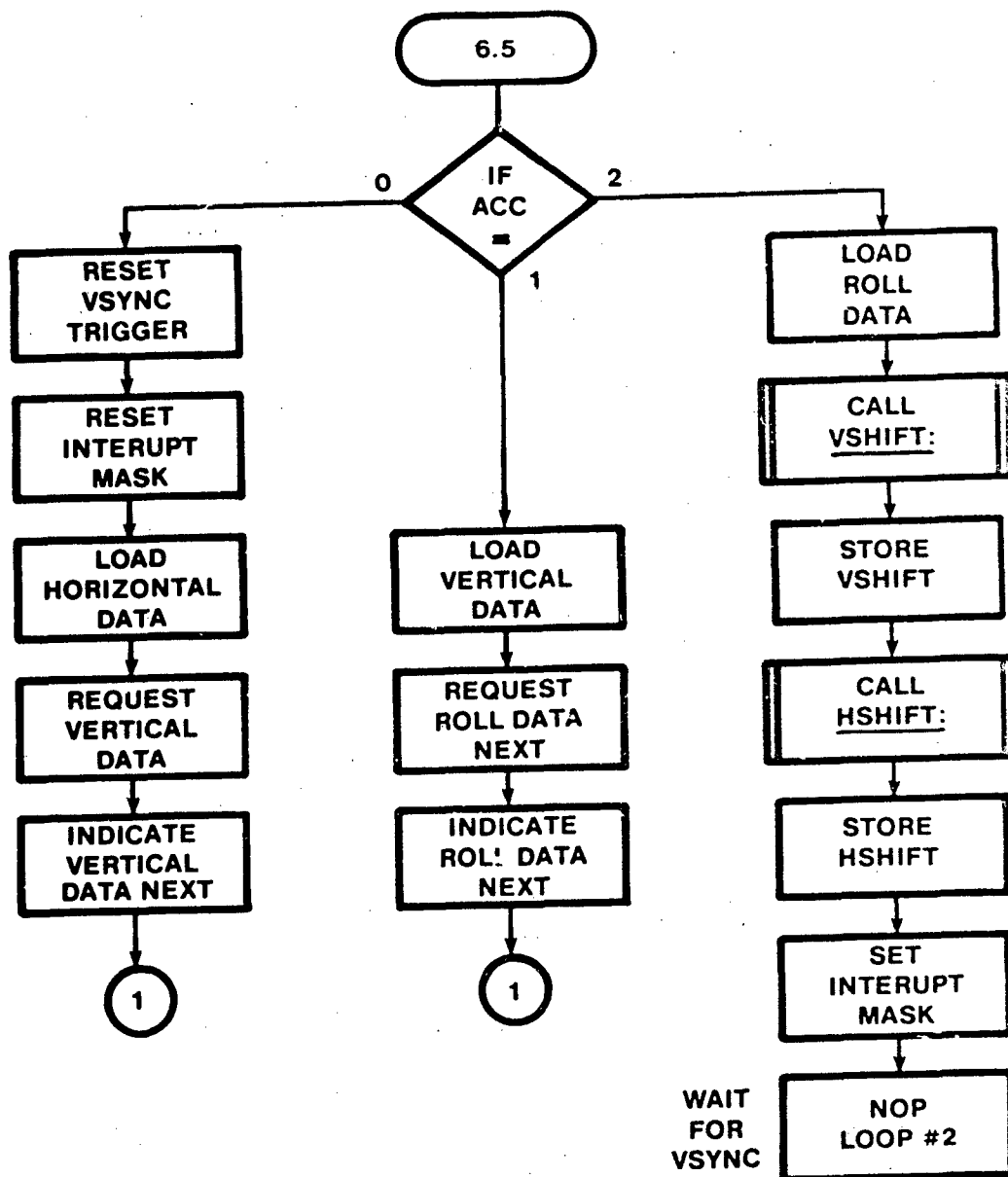
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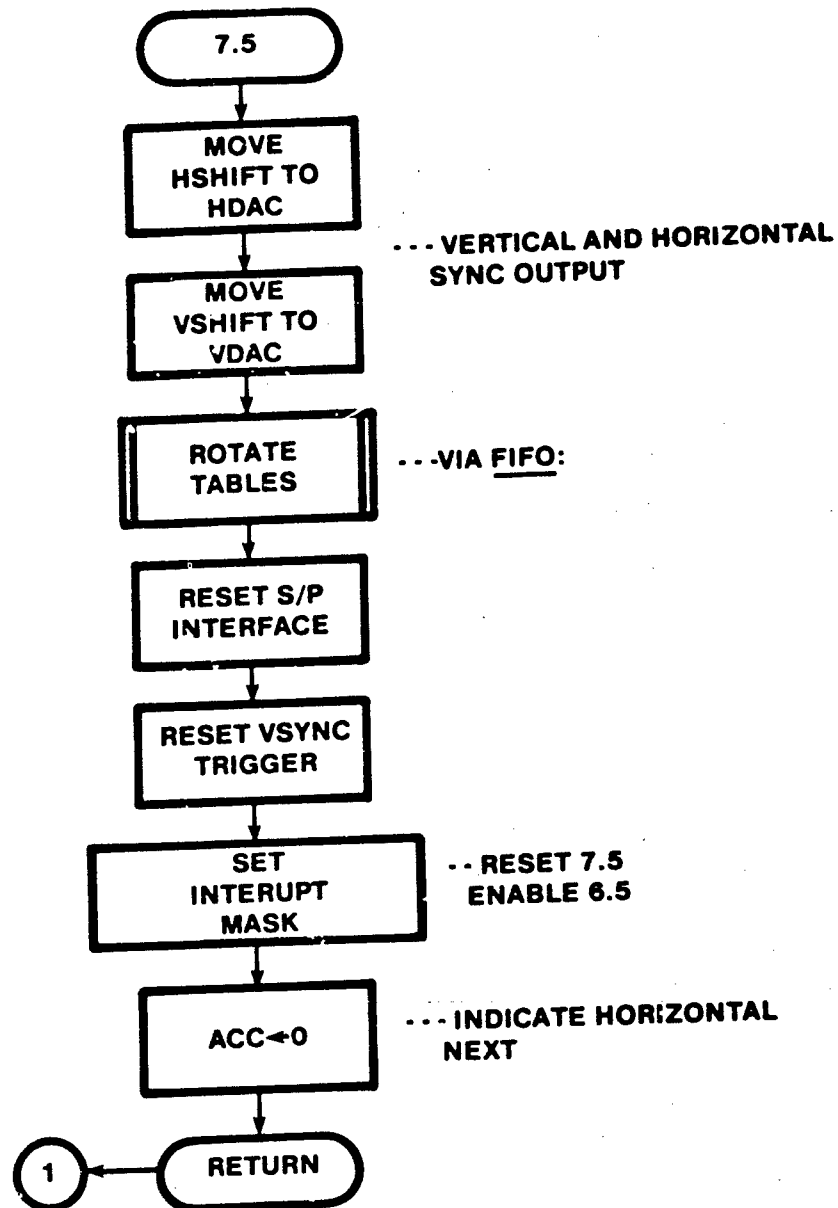
WHERE N IS A CONTROL VALUE WITH AN ALLOWED RANGE OF $\leftarrow 21$ FOR EACH INDIVIDUAL OFFSET (SEE SUBROUTINE ADJUST).

THE SHIFTING OF THE RASTER IS ACCOMPLISHED BY CHANGING THE VERTICAL AND HORIZONTAL SYNC SIGNALS DURING THE VERTICAL RETRACE TIME. THE AMOUNT OF OFFSET IS LIMITED BY MAXX AND MAXY VALUES WHICH SHOULD BE SET AT A MAXIMUM OF 82 DECIMAL. BEFORE RUNNING THIS PROGRAM BE CERTAIN THAT THE RESERVED RAM LOCATIONS ARE FILLED WITH THE PROPER INFORMATION THAT DEFINE THE STORAGE TABLES, CONTROL VALUES, AND MAXIMUM SHIFT VALUES. THIS MAY BE DONE VIA SUBROUTINES INT4, INT5, OR INT6.

NTHPREV







NAVTRAEQUIPCEN IH-338

I-15-II 8000/8005 MACRO ASSEMBLER, V3.0

LPREV

LOC	OBJ	LINE	SOURCE STATEMENT
		47 ,	
		48 ;	
		49	EXTRN TBSUB, DIV32, DIV16, ADJUST, TBRDD, MAX, TBLSET, FIFO, PEGOUT
		50	EXTRN MESS, STOREL, STK, INPUTS, HINITL, VINITL, HSRC, VSRC, HFINAL, VFINAL
		51	EXTRN HCONTR, VCONTR, HCENTR, VCENTR, HZERO, VZERO, HMAX, VMAX, SCRCH1, SCRCH2
		52	EXTRN HINPUT, VINPUT, RINPUT, GETELV, RSTSP, VSYNC, HDAC, VDAC, FIRST
		53	EXTRN PST650, PST65A, RST75E, PST750
		54 ,	
		55	REJECT

NAVTRAEQUIPCEN IH-338

1515-11 0000/0005 MACRO ASSEMBLER, V3.0

LPREV

LOC	OBJ	LINE	SOURCE STATEMENT
		56	CSEG
0000	F3	57	LPREV: DI
0001	310000	58	LXI SP, STK
		59	
0004	210000	60	LXI H, FIRST
0007	220000	61	SHLD RST658
000A	215400	62	LXI H, MNSEG
000D	220000	63	SHLD RST65A
		64	
0010	210000	65	LXI H, FIRST
0013	220000	66	SHLD RST75E
0016	21C200	67	LXI H, OUTPUT
0019	220000	68	SHLD RST750
		69	
001C	2A0000	70	LHLD HZERO
001F	EB	71	XCHG
0020	2A0000	72	LDA HFINAL
0023	2A0000	73	LHLD HINITL
0026	CD0000	74	CALL TBLSET
0029	2A0000	75	LHLD VZERO
002C	EB	76	XCHG
002D	2A0000	77	LDA VFINAL
0030	2A0000	78	LHLD VINITL
0033	CD0000	79	CALL TBLSET
		80	
0036	2A0000	81	LDA HCENTR
0039	320000	82	STA HDAC
003C	2A0000	83	LDA VCENTR
003F	320000	84	STA VDAC
		85	
0042	320000	86	STA RSTSP
0045	320000	87	STA VSYNC
0048	3E00	88	MVI A, 10H
004A	20	89	SIM
		90	
		91	
004E	2E00	92	MVI A, 00H
0040	F3	93	EI
004E	00	94	LOOP1: NOP
004F	00	95	NOP
0050	00	96	NOP
0051	C34E00	97	JMP LOOP1
		98	
		99	MNSEG: ***** MAIN SEGMENT *****
0054	FE01	100	CPI 01H
0056	CD2000	101	JZ VERT
0059	FE02	102	CPI 02H
005B	CD0000	103	JZ ROLL
		104	REJECT

NAVTRAEQUIPCEN IH-338

IS15-II 0000/0005 MACRO ASSEMBLER, V3 0

LPREV

LOC	OBJ	LINE	SOURCE STATEMENT
		105 ;	
		106 ;	
		107 RSET:	; SET UP TO GRAB NEXT VSYNC
		108 ;	
005E	320000	E 109	STA VSYNC ; RESET VSYNC TRIGGER
		110 ;	
0061	3E1D	111	MVI A, 10H
0063	30	112	SIM ; RESET 7.5. ENABLE 6.5
		113 ;	
0064	2A0000	E 114	HORIZ: LHLD HINPUT
0067	EB	115	XCHG
0068	2A0000	E 116	LHLD HINITL ; (D,E) - DATA FROM PORT ; (H,L) - HINITIAL ADDRESS
006B	73	117	MOV M, E
006C	23	118	INX H
006D	7A	119	MOV A, D ; ACC GETS HI BYTE OF HINPUT
006E	17	120	RAL
006F	3F	121	CNC ; COMPLIMENT MSB OF HINPUT
0070	1F	122	RAR
0071	77	123	MOV M, A ; STORE HI BYTE OF HINPUT IN HTABLE
0072	320000	E 124	STA GETELV ; SEND GET ELEVATION SIGNAL
0075	3E01	125	MVI A, 01H ; INDICATE VERTICAL DATA NEXT
0077	FB	126	EI ; ENABLE INTERRUPTS
0078	C9	127	RET ; AND RETURN TO LOOP1
		128 ;	
0079	2A0000	E 129	VERT: LHLD VINPUT ; VERTICAL INPUT SEGMENT
007C	EB	130	XCHG ; (D,E) - VERTICAL DATA
007D	2A0000	E 131	LHLD VINITL ; (H,L) - VINITIAL ADDRESS
0080	73	132	MOV M, E ; STORE LO BYTE OF VINPUT
0081	23	133	INX H ; POINT TO NEXT LOCATION
0082	7A	134	MOV A, D
0083	17	135	RAL
0084	3F	136	CNC ; COMPLIMENT MSB OF VINPUT
0085	1F	137	RAR
0086	77	138	MOV M, A ; STORE HI BYTE IN VTABLE
0087	3E02	139	MVI A, 02H ; INDICATE ROLL DATA NEXT
0089	320000	E 140	STA GETELV ; REQUEST ROLL DATA FROM PHT
008C	FB	141	EI ; ENABLE INTERRUPTS
008D	C9	142	RET ; RETURN TO LOOP 01
		143 ;	
008E	2A0000	E 144	ROLL: LHLD RINPUT ; ROLL INPUT SECTION
0091	EB	145	XCHG ; (D,E) GETS ROLL DATA
0092	211E20	146	LXI H, 201EH ; (H,L) CONTAINS STORAGE ADDRESS
0095	73	147	MOV M, E ; STORE LO-BYTE OF ROLL
0096	23	148	INX H ; POINT TO MEM. 201F
0097	7A	149	MOV A, D
0098	17	150	RAL
0099	3F	151	CNC ; COMPLIMENT MSB OF RINPUT
009A	1F	152	RAR
009B	77	153	MOV M, A ; STORE HI-BYTE OF RINPUT
		154	#EJECT

NAVTRAEQUIPCEN IH-338

1515-11 0000/0005 MACRO ASSEMBLER V3.0

LPREV

LOC	OBJ	LINE	SOURCE STATEMENT
		155	CALCULATE SHIFT VALUES (VERTICAL AND HORIZONTAL ONLY)
		156	
009C	2A0000	E 157	LHLD VINITL
009F	EB	158	XCHG
00A0	2A0000	E 159	LHLD VFINAL
00A3	2B	160	DCX H
00A4	CD700	C 161	CALL VSHIFT
00A7	F5	162	PUSH PSW
		163	
00A8	2A0000	E 164	LHLD HINITL
00AB	EB	165	XCHG
00AC	2A0000	E 166	LHLD HFINAL
00AF	2B	167	DCX H
00B0	CD2701	C 168	CALL HSHIFT
00B3	F5	169	PUSH PSW
		170	
00B4	3E08	171	MVI A,08H
00B6	30	172	SIM
		173	
00B7	F1	174	POP PSW
00B8	FB	175	EI
		176	
00B9	00	177	LOOP2: NOP
00BA	320500	178	STA 0005H
00BD	00	179	NOP
00BE	00	180	NOP
00BF	C38900	C 181	JMP LOOP2
		182	
		183	OUTPUT:
		184	
00C2	E1	185	POP H
00C3	320000	E 186	STA HDAC
		187	
00C6	F1	188	POP PSW
00C7	320000	E 189	STA VDAC
		190	#EJECT

NAVTRAEQUIPCEN IH-338

1515-11 0000/0005 MACRO ASSEMBLER, V3 0

LPREV

LOC	OBJ	LINE	SOURCE STATEMENT	
		191	ROTATE	; SET UP FOR NEXT CYCLE
00CA	3A0000	E 192	LDA HINITL	
00CD	47	193	MOV B, A	; B GETS HINITIAL ADDRESS (LO)
00CE	2A0000	E 194	LHLD HSRC	
00D1	EB	195	XCHG	; (D, E) GETS HSOURCE ADDRESS
00D2	2A0000	E 196	LHLD HFINAL	; (H, L) GETS HFINAL ADDRESS
00D5	CD0000	E 197	CALL FIFO	; ROTATE HTABLE
		198 ;		
00D8	3A0000	E 199	LDA VINITL	
00DB	47	200	MOV B, A	; B GETS VINITIAL ADDRESS (LO)
00DC	2A0000	E 201	LHLD VSRC	
00DF	EB	202	XCHG	; (D, E) GETS VSOURCE ADDRESS
00E0	2A0000	E 203	LHLD VFINAL	; (H, L) GETS VFINAL ADDRESS
00E3	CD0000	E 204	CALL FIFO	; ROTATE VTABLE
		205 ;		
		206 ;		
00E6	320000	E 207	STA PSTSP	; RESET SERIAL TO PARALLEL INTERFACE
		208 ;		
00E9	3E00	209	MVI A, 00H	
00EB	30	210	SIM	; ENABLE 6.5 INTERRUPT
00EC	00	211	NOP	
00ED	00	212	NOP	
00EE	00	213	NOP	
00EF	00	214	NOP	
00F0	00	215	NOP	
00F1	00	216	NOP	
00F2	00	217	NOP	
00F3	3E00	218	MVI A, 00H	; INDICATE HORIZONTAL NEXT
		219 ;		
00F5	FB	220	EI	; ENABLE INTERRUPTS
00F6	C9	221	RET	; RETURN TO LOOP1 VIA 6.5 RETURN
		222 ;		
		223	\$TITLE (' VSHIFT ')	
		224	\$EJECT	

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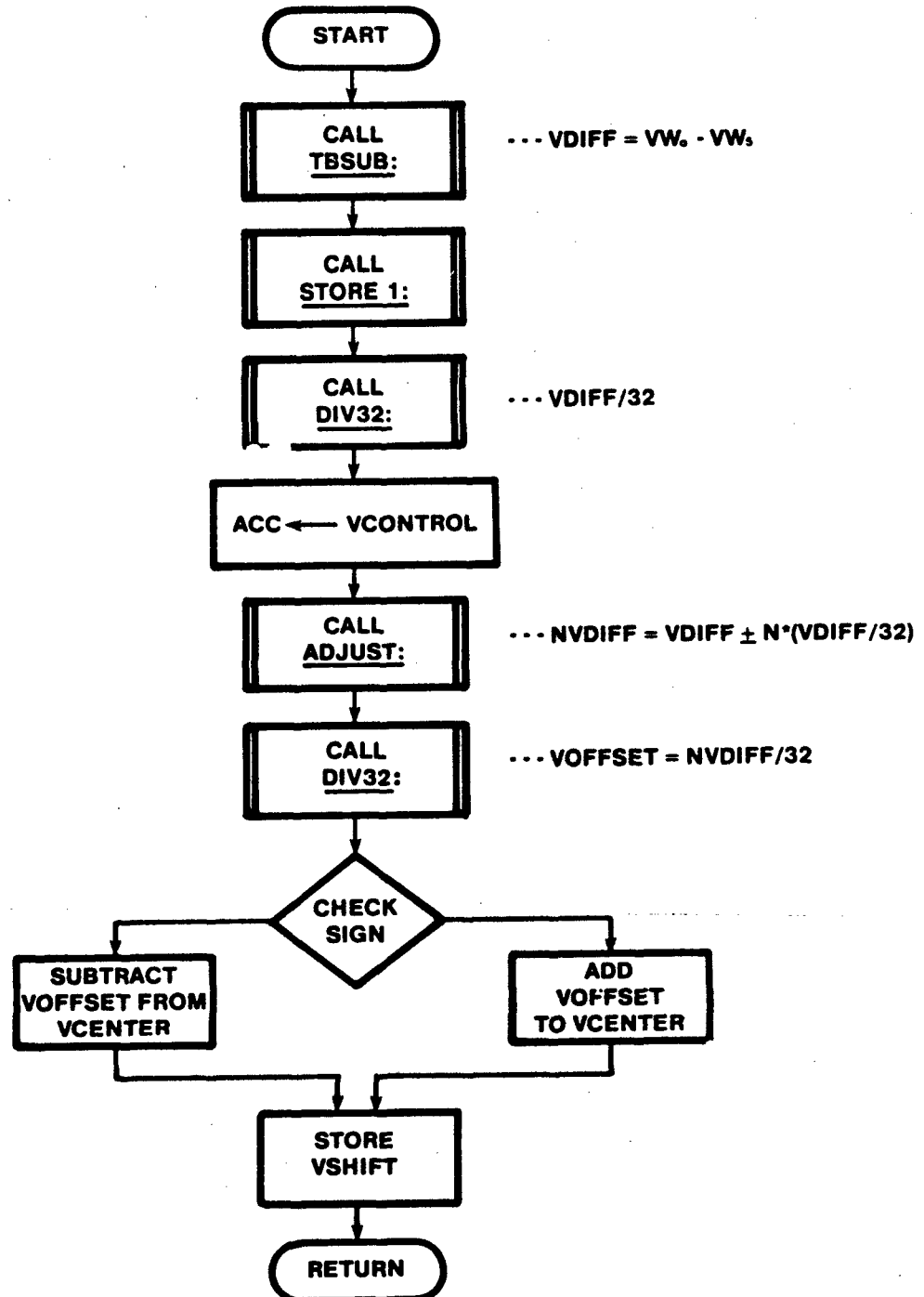
IS15-11 8888/8885 MACRO ASSEMBLER, V3.0 LPREV
VSHIFT

```

LOC  OBJ      LINE      SOURCE STATEMENT
225 ;
226 ;
227 ;
228 ;          *****
229 ;          *          *
230 ;          *   VSHIFT   *
231 ;          *          *
232 ;          *****
233 ;
234 ;          MODIFIED FOR LASER PROJECTOR JULY 2 1991
235 ;
236 ;          VSHIFT IS USED TO CALCULATE THE VERTICAL SHIFT VALUE TO BE SENT TO THE VERTICAL DAC
237 ;
238 ;          VSHIFT = VCENTER - VOFFSET
239 ;
240 ;          VOFFSET = VDIFF +- N * (VDIFF/16)
241 ;
242 ;          32
243 ;
244 ;
245 ;          VSHIFT USES SUBROUTINES : TBSUB, STORE1, DIV32, DIV16, ADJUST, MAX.
246 ;
247 ;
248 ; INPUTS:
249 ;          (D,E) CONTAINS THE ADDRESS OF V WORD 0;
250 ;          (H,L) CONTAINS THE ADDRESS OF V WORD FINAL
251 ;          BOTH WORDS ARE TWO BYTE
252 ;
253 ;          VCENTER, VMAX, AND VCONTROL MUST BE IN THEIR PROPER LOCATION IN RAM
254 ;
255 ; OUTPUTS:
256 ;          NVDIFF AT SCRCH1 ( VDIFF +- VCONTROL*VDIFF/16 )
257 ;          HOFFSET AT SCRCH2 ( NVDIFF/32 )
258 ;          THE SIGN OF NVDIFF, VOFFSET IS STORED AT (H,L) + 2
259 ;          VSHIFT IS IN THE ACC. AND AT (H,L) + 3
260 ;
261 $EJECT

```

SUBROUTINE VSHIFT



NAVTRAEQUIPCEN IH-338

ISIS-II 0000/0005 MACRO ASSEMBLER, V3.0
VSHIFT

LPREV

LOC	OBJ	LINE	SOURCE STATEMENT
		262 ;	
		263 ;	
		264	CSEG
		265	VSHIFT:
00F7	E5	266	PUSH H
00F8	CD0000	267	CALL TBSUB
00F8	CD0000	268	CALL STORE1
00FE	CD0000	269	CALL DIV16
		270 ;	
0101	3A0000	271	LDA VCONTR
0104	CD0000	272	CALL ADJUST
		273 ;	
0107	CD0000	274	CALL DIV32
		275 ;	
010A	3A0000	276	LDA VMAX
010D	CD0000	277	CALL MAX
		278 ;	
0110	3A0000	279	LDA VCENTER
0113	4F	280	MOV C,A
0114	E1	281	POP H
0115	23	282	INX H
0116	23	283	INX H
0117	7E	284	MOV A,H
0118	FE00	285	CPI 00H
011A	CA2201	286	JZ MINUS
		287 ;	
		288 ;	
		289	IF SIGN IS NOT ZERO ADD (PLUS, MINUS, AND FINISH ARE USED BY VSHIFT AND HSHIFT)
		290 ;	
		291 PLUS:	
011D	79	292	MOV A,C
011E	00	293	ADD B
011F	C32401	294	JMP FINISH
		295 ;	
		296 MINUS:	
0122	79	297	MOV A,C
0123	90	298	SUB B
		299 ;	
		300 FINISH:	
0124	23	301	INX H
0125	77	302	MOV H,A
		303 ;	
0126	C9	304	RET
		305 ;	
		306 ;	
		307	BTITLE (' HSHIFT ')
		308	EJECT

SAVE (H,L)-Y WORD FINAL ADDRESS
FIND VDIFF
STORE VDIFF AT SCRATCH
VDIFF/16
ACC GETS VCONTROL
NVDIFF=VDIFF + N*(VDIFF/16)
VOFFSET = NVDIFF/32
ACC GETS MAXIMUM OFFSET
CHECK FOR MAXIMUM SHIFT VALUE
C GETS VCENTER VALUE
WORD FINAL ADDRESS OFF 57K
(H,L) POINTS TO SIGN ADDRESS
ACC GETS SIGN(0-POS, 1-NEG.)
COMPARE SIGN WITH ZERO
IF SIGN IS POSITIVE SUBTRACT
VOFFSET FROM VCENTER
ACC GETS CENTER VALUE
ADD OFFSET TO CENTER
FINISH UP SUBROUTINE
ACC GETS CENTER VALUE
SUBTRACT OFFSET FROM CENTER
POINT PAST SIGN OF DIFF
STORE SHIFT VALUE
RETURN TO CALLING PROGRAM

NAVTRAEQUIPCEN IH-338

ISIS-II 8080/8085 MACRO ASSEMBLER, V3.0

LPREV

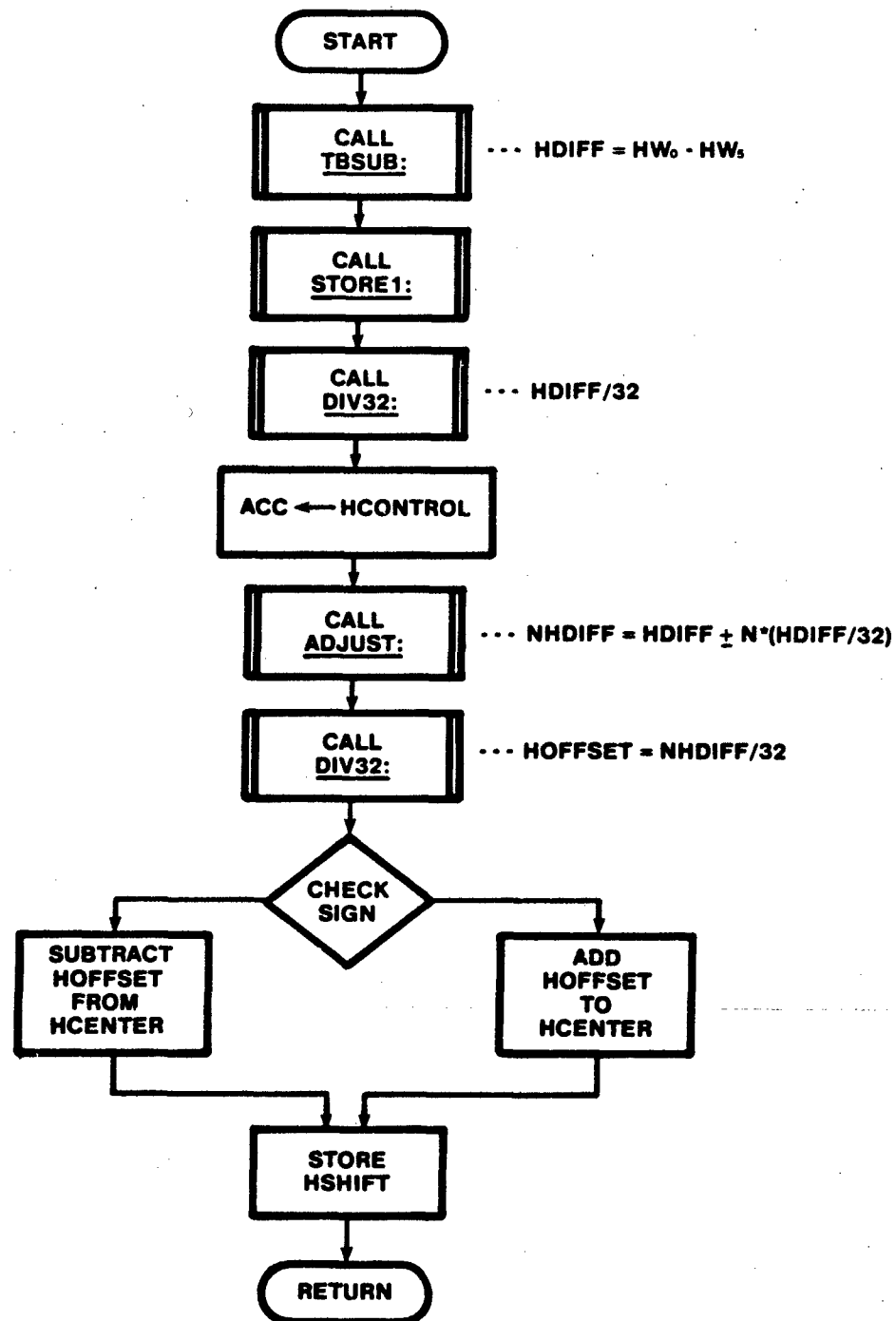
MSHIFT

```

LOC  OBJ      LINE      SOURCE STATEMENT
309 ;
310 ;
311 ;
312 ;
313 ;          *****
314 ;          *                *
315 ;          *      HSHIFT      *
316 ;          *                *
317 ;          *****
318 ;
319 ;      MODIFIED FOR LASER PROJECTOR JULY 2 1981
320 ;
321 ;
322 ;      HSHIFT IS USED TO CALCULATE THE HORIZONTAL SHIFT VALUE TO BE SENT TO THE H0AC
323 ;
324 ;          HSHIFT = H0CENTER - H0FFSET
325 ;
326 ;          H0FFSET = H0DIFF + N * (H0DIFF/16)
327 ;
328 ;
329 ;
330 ;
331 ;      HSHIFT USES SUBROUTINES: TBSUB, DIV32, DIV16, ST0PEL, ADJUST, MAX, PLUS, MINUS, FINISH
332 ;
333 ;      INPUTS:
334 ;          (D,E)- CONTAINS THE ADDRESS OF H WORD 0
335 ;          (H,L)- CONTAINS THE ADDRESS OF H WORD FINAL
336 ;          BOTH WORDS ARE 2-BYTE
337 ;
338 ;          H0CENTER, HMAX, AND H0CONTROL MUST BE IN THEIR PROPER LOCATION IN RAM
339 ;
340 ;      OUTPUTS:
341 ;          N0DIFF AT SC0RCH1 (H0DIFF + H0CONTROL+H0DIFF/16)
342 ;          H0FFSET AT SC0RCH2 ( N0DIFF/32 )
343 ;          THE SIGN OF H0FFSET, N0DIFF IS STORED AT (H,L) + 2
344 ;          HSHIFT IS IN THE ACCUMULATOR AND AT (H,L) + 3
345 ;
346 ;      $EJECT

```


SUBROUTINE HSHIFT



NAVTRAEQUIPCEN IH-338

ISIS-II 8080/8085 MACRO ASSEMBLER, V3.0
HSHIFT

LPREV

LOC	OBJ	LINE	SOURCE STATEMENT	
		347 ;		
		348 ;		
		349	CSEG	
		350 HSHIFT:		
0127	E5	351	PUSH H	; (H,L) SAVED IN STK
0128	CD0000	E 352	CALL TBSUB	; CALCULATE HDIFF
0128	CD0000	E 353	CALL STORE1	; STORE HDIFF AT SCRATCH1
		354 ;		
012E	CD0000	E 355	CALL DIV16	; HDIFF/16
		356 ;		
0131	3A0000	E 357	LDA HCONTR	; ACC GETS HCONTROL VALUE
0134	CD0000	E 358	CALL ADJUST	; HDIFF=HDIFF+1*(HDIFF/16)
		359 ;		
0137	CD0000	E 360	CALL DIV32	; HOFFSE. = HDIFF/32
		361 ;		
013A	3A0000	E 362	LDA HMAX	; ACC GETS MAXIMUM H SHIFT VALUE
013D	CD0000	E 363	CALL MAX	; DETERMINE IF MAX IS REACHED
		364 ;		LEAVE HOFFSET IN B REGISTER
0140	3A0000	E 365	LDA HCENTR	
0143	4F	366	MOV C, A	; C GETS H CENTER VALUE
0144	E1	367	POP H	; H WORD FINAL ADDRESS OFF STK
0145	23	368	INX H	
0146	23	369	INX H	; (H,L) POINTS TO H SIGN LOCATION
0147	7E	370	MOV A, M	; ACC GETS SIGN VALUE (0-POS, 1-NEG)
0148	FE00	371	CPI 00H	; COMPARE SIGN WITH ZERO
014A	CA2201	C 372	JZ MINUS	; IF SIGN IS POSITIVE SUBTRACT
		373 ;		VIA MINUS THEN FINISH SUBROUTINE
		374 ;		
		375 ;	IF SIGN IS POSITIVE ADD HCENTER TO HOFFSET	
		376 ;		
014D	C31D01	C 377	JMP PLUS	; ADD THEN FINISH SUBROUTINE
		378 ;		
		379 \$EJECT		

NAVTRAEQUIPCEN IH-338

IS15-II 8000/8085 MACRO ASSEMBLER, V3.0
HSHIFT

LPREV

LOC	OBJ	LINE	SOURCE STATEMENT
		398	END

PUBLIC SYMBOLS

EXTERNAL SYMBOLS

ADJUST E 0000	DIV16 E 0000	DIV32 E 0000	FIFO E 0000	FIRST E 0000	GETELY E 0000	HCENTP E 0000
HCONTR E 0000	HDAC E 0000	HFINAL E 0000	HINITL E 0000	HINPUT E 0000	HMAX E 0000	HSRC E 0000
HZERO E 0000	INPUTS E 0000	MAX E 0000	MESS E 0000	REGOUT E 0000	RINPUT E 0000	RST650 E 0000
RST65A E 0000	RST750 E 0000	RST75E E 0000	RSTSP E 0000	SCRCH1 E 0000	SCRCH2 E 0000	STK E 0000
STORE1 E 0000	TBADD E 0000	TBLSET E 0000	TBSUB E 0000	VCENTR E 0000	VCONTR E 0000	VDAC E 0000
VFINAL E 0000	VINITL E 0000	VINPUT E 0000	VMAX E 0000	VSRC E 0000	VSNC E 0000	VZERO E 0000

USER SYMBOLS

ADJUST E 0000	DIV16 E 0000	DIV32 E 0000	FIFO E 0000	FINISH C 0124	FIRST E 0000	GETELY E 0000
HCONTR E 0000	HCONTR E 0000	HDAC E 0000	HFINAL E 0000	HINITL E 0000	HINPUT E 0000	HMAX E 0000
HORIZ C 0064	HSHIFT C 0127	HSRC E 0000	HZERO E 0000	INPUTS E 0000	LOOP1 C 004E	LOOP2 C 0089
LPREV C 0000	MAX E 0000	MESS E 0000	MINUS C 0122	MINSEG C 0054	OUTPUT C 00C2	PLUS C 011D
REGOUT E 0000	RINPUT E 0000	ROLL C 008E	ROTATE C 00CA	RSET C 005E	RST650 E 0000	RST65A E 0000
RST750 E 0000	RST75E E 0000	RSTSP E 0000	SCRCH1 E 0000	SCRCH2 E 0000	STK E 0000	STORE1 E 0000
TBADD E 0000	TBLSET E 0000	TBSUB E 0000	VCENTR E 0000	VCONTR E 0000	VDAC E 0000	VERT C 0079
VFINAL E 0000	VINITL E 0000	VINPUT E 0000	VMAX E 0000	VSHIFT C 00F7	VSRC E 0000	VSNC E 0000
VZERO E 0000						

ASSEMBLY COMPLETE. NO ERRORS

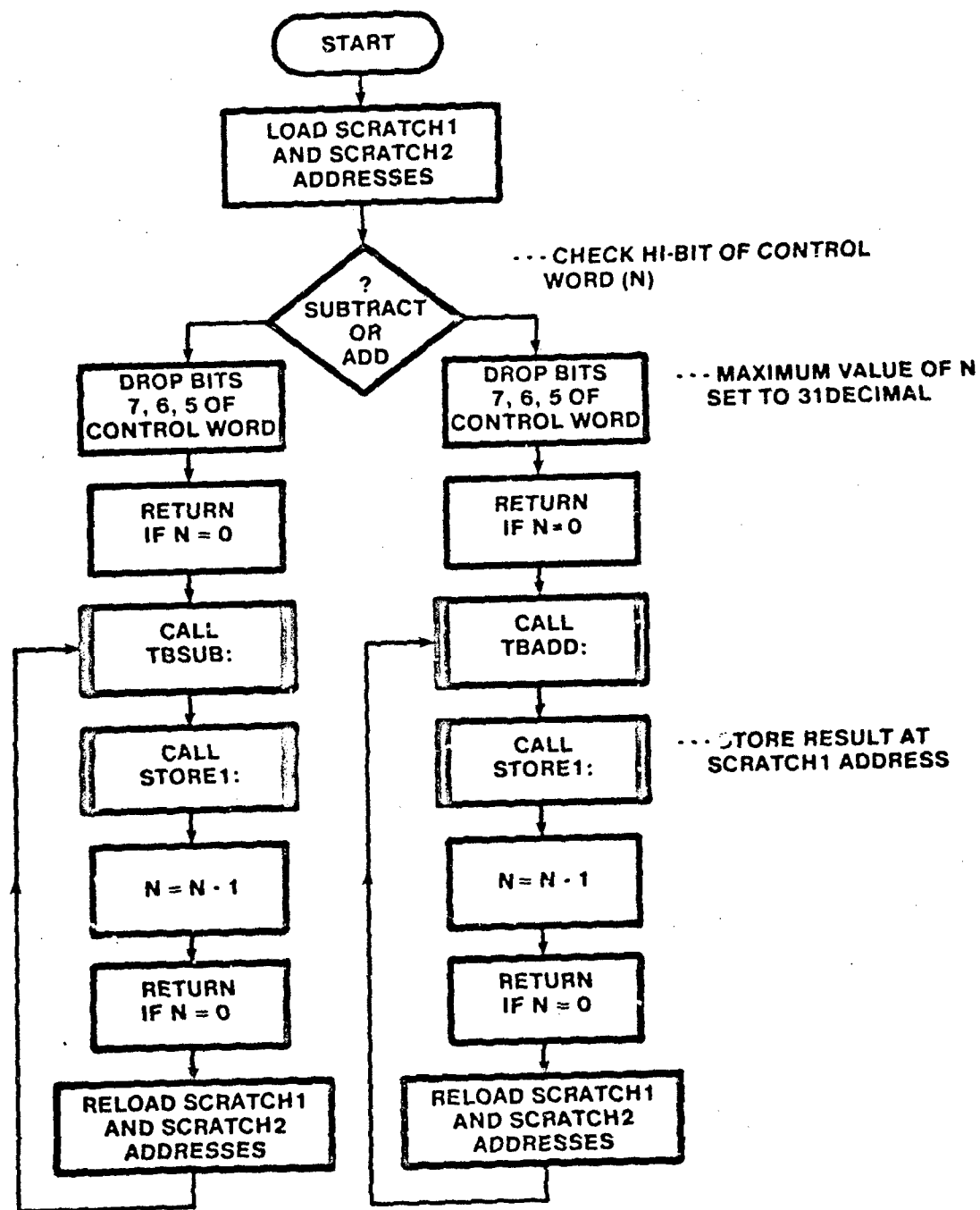
NAVTRAEQUIPCEN IH-338

ISIS-II 8000/8005 MACRO ASSEMBLER, V3 0
ADJUST

SUB5

LOC	OBJ	LINE	SOURCE STATEMENT
373			;
374			*****
375			* *
376			* ADJUST *
377			* *
378			*****
379			;
380			;
381			THIS SUBROUTINE EVALUATES THE MATHEMATICAL EXPRESSION
382			
383			$Z = X + (N * Y)$
384			;
385			WHERE X AND Y ARE TWO BYTE WORDS STORED AT RAM LOCATIONS SCRATCH1 AND
386			SCRATCH2, RESPECTIVLY N IS A VARIABLE WHICH IS PASSED TO THE
387			SUBROUTINE IN THE ACCUMULATOR ; N HAS AN ALLOWABLE RANGE OF +- 31
388			WITH THE SIGN INDICATED BY THE MSB (BIT 7) OF THE ACC. SET TO 0 FOR
389			POSITIVE OR 1 FOR NEGATIVE.
390			;
391			THE RESULT Z IS STORED AT THE ORIGINAL LOCATION OF X (SCRATCH 1)
392			;
393			;
394			INPUTS:
395			ACC CONTAINS THE VARIABLE WORD N
396			MSB - X X - - - - - LSB - N
397			7 6 5 4 3 2 1 0 BIT 0
398			5 <--RANGE--> = 31
399			I
400			G
401			N [IF BIT#7 = 0, N IS POSITIVE]
402			[IF BIT#7 = 1, N IS NEGATIVE]
403			** BITS 6 AND 5 ARE NOT USED (AND VALUE 1 IF HEX DROPS THEM)
404			;
405			X IS CONTAINED IN RAM LOCATIONS SCRATCH1, SCRATCH1 + 1
406			;
407			Y IS CONTAINED IN RAM LOCATIONS SCRATCH2, SCRATCH2 + 1
408			;
409			;
410			OUTPUT:
411			Z IS CONTAINED IN RAM LOCATIONS: SCRATCH1 (LO) AND SCRATCH1 + 1 (HI)
412			;
413			\$EJECT

ADJUST



$$\text{RESULT} = \text{SCRATCH1} \pm N * \text{SCRATCH2}$$

NAVTRAEQUIPCEN IH-338

ISIS-II 0000/0005 MACRO ASSEMBLER V3.0
ADJUST

SUBS

LOC	OBJ	LINE	SOURCE STATEMENT	
		414	CSEG	
		415	ADJUST	
000A	110000	E 416	LXI D, SCRCH1	; (D, E) CONTAIN ADDRESS OF X
000D	210000	E 417	LXI H, SCRCH2	; (H, L) CONTAIN ADDRESS OF Y
		418		
0090	17	419	RAL	; ROTATE BIT 7 TO CARRY POSITION
0091	DAAC00	C 420	JC NEG	; IF CARRY IS SET, N IS NEGATIVE
		421		
		422	POS	
0094	0F	423	RRC	; RESTORE ACCUMULATOR
0095	E61F	424	ANI 1FH	; REMOVE BITS 7, 6, 5 (SET RANGE TO 31)
0097	C8	425	RZ	; RETURN IF N = 0
0098	F5	426	PUSH PSH	; SAVE COUNTER (I)
		427	XPLUSV	
0099	CD6F00	C 428	CALL TBADD	; Z = X + Y
009C	CD8200	C 429	CALL STORE1	; X = Z (Z IS STORED AT Y'S ADDRESS)
009F	F1	430	POP PSH	
00A0	3D	431	DCR A	; I = I - 1 (DECREMENT COUNTER)
00A1	C8	432	RZ	; RETURN IF COUNTER = 0
00A2	F5	433	PUSH PSH	; IF COUNTER > 0, THEN
00A3	110000	E 434	LXI D, SCRCH1	; RELOAD X AND Y ADDRESSES
00A6	210000	E 435	LXI H, SCRCH2	
00A9	C39900	C 436	JMP XPLUSV	; ADD Y TO X AGAIN
		437		
		438	NEG	
00AC	0F	439	RRC	; RESTORE ACCUMULATOR
00AD	E61F	440	ANI 1FH	; REMOVE BITS 7, 6, 5 (SET RANGE TO 31)
00AF	C8	441	RZ	; RETURN IF N = 0
00B0	F5	442	PUSH PSH	; SAVE COUNTER (I)
		443	XMINUSV	
00B1	CD3200	C 444	CALL TBSUB	; Z = X - Y
00B4	CD8200	C 445	CALL STORE1	; X = Z (Z IS STORED AT X'S ADDRESS)
00B7	F1	446	POP PSH	
00B8	3D	447	DCR A	; I = I - 1 (DECREMENT COUNTER)
00B9	C8	448	RZ	; RETURN IF COUNTER = 0
00BA	F5	449	PUSH PSH	; IF COUNTER > 0, THEN
00BB	110000	E 450	LXI D, SCRCH1	; RELOAD X AND Y ADDRESSES
00BE	210000	E 451	LXI H, SCRCH2	
00C1	C38100	C 452	JMP XMINUSV	; SUBTRACT Y FROM X AGAIN
		453		
		454	\$TITLE ('TABLE.SET')	
		455	\$EJECT	

NAVTRAEQUIPCEN IH-338

ASH80 F1 PHTMAP SPC DEBUG MODES

1515-11 0000/0005 MACRO ASSEMBLER V3 0

PHTMAP

LOC OBJ LINE SOURCE STATEMENT

1
2
3 NAME PHTMAP

```

*****
*
*   PHTMAP
*
*****

```

THIS PROGRAM IS DESIGNED TO TEST THE POLHEMUS HEAD TRACKER SHMS-III-A IN CONJUNCTION WITH AN INTERFACE BOARD THAT CONVERTS THE PHT'S SERIAL DATA TO PARALLEL DATA

THE PROGRAM INITIALLY RESETS THE S/P BOARD, WHICH CAUSES A REQUEST FOR POLHEMUS TO CALCULATE A NEW SET OF DATA. THEN A LOOP IS ENCOUNTERED WHERE THE PROGRAM WAITS FOR A DATA READY SIGNAL (6 5 INTERRUPT). WHEN DATA READY IS SENT, THE NEXT PART OF THE PROGRAM STORES A WORD OF DATA. THE WORD STORED DEPENDS ON THE VALUE STORED IN THE C-REGISTER

00H - HORIZONTAL DATA (AZIMUTH)
01H - VERTICAL DATA (ELEVATION)
02H - ROLL DATA

THIS STORAGE CONTINUES UNTIL THE RAM USED FOR STORAGE IS FILLED (RAM 2000H - 20FFH) SINCE EACH PHT WORD IS TWO-BYTE THE PROGRAM STORES 128 VALUES OF DATA. AFTER 128 VALUES ARE STORED THE PROGRAM DROPS OUT OF THE STORE MODE AND INTO THE NON-STORE MODE. IN THIS MODE, THE SAME TYPE OF DATA, AS INDICATED BY THE C-REGISTER, IS PULLED ONTO THE INPUT PORTS BUT IS NOT STORED. WHEN THIS DATA IS ON THE PORT, THE BIT PATTERN CAN BE READ FROM LED'S ON THE S/P BOARD. IN ORDER TO SEE THESE BIT PATTERNS, A DELAY LOOP IS ENTERED TO WAIT BEFORE PULLING IN NEW DATA, ALLOWING THE DATA TO BE ON THE PORT LONG ENOUGH TO CAUSE THE LED'S TO REMAIN LIGHTED AND TO ALLOW ONE TO SEE THE BIT PATTERN

DEFINE CONSTANTS

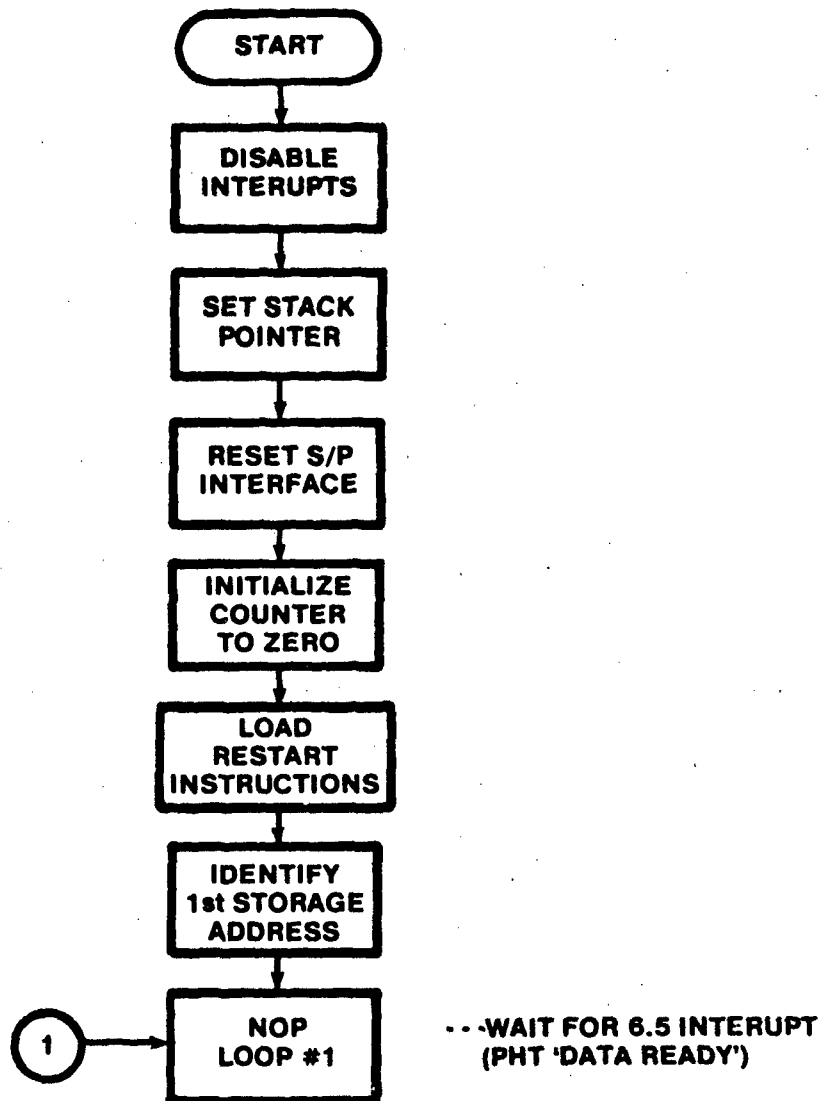
03F1	41 DELAY	EQU	03F1H	; ADDRESS OF MONITOR DELAY ROUTINE
2000	42 COUNT	EQU	2000H	; DELAY COUNT VALUE (APPROX. SEC.)
001D	43 MASK	EQU	1DH	; 5TH MASK VALUE
00FF	44 ENDSTO	EQU	0FFH	; END OF STORAGE VALUE
2000	45 BEGIN	EQU	2000H	; BEGINNING OF STORAGE

DEFINE EXTERNAL VALUES

EXTRN RST638, RST63A, HINPUL, GETELY, RSTSP, STK, FIRST

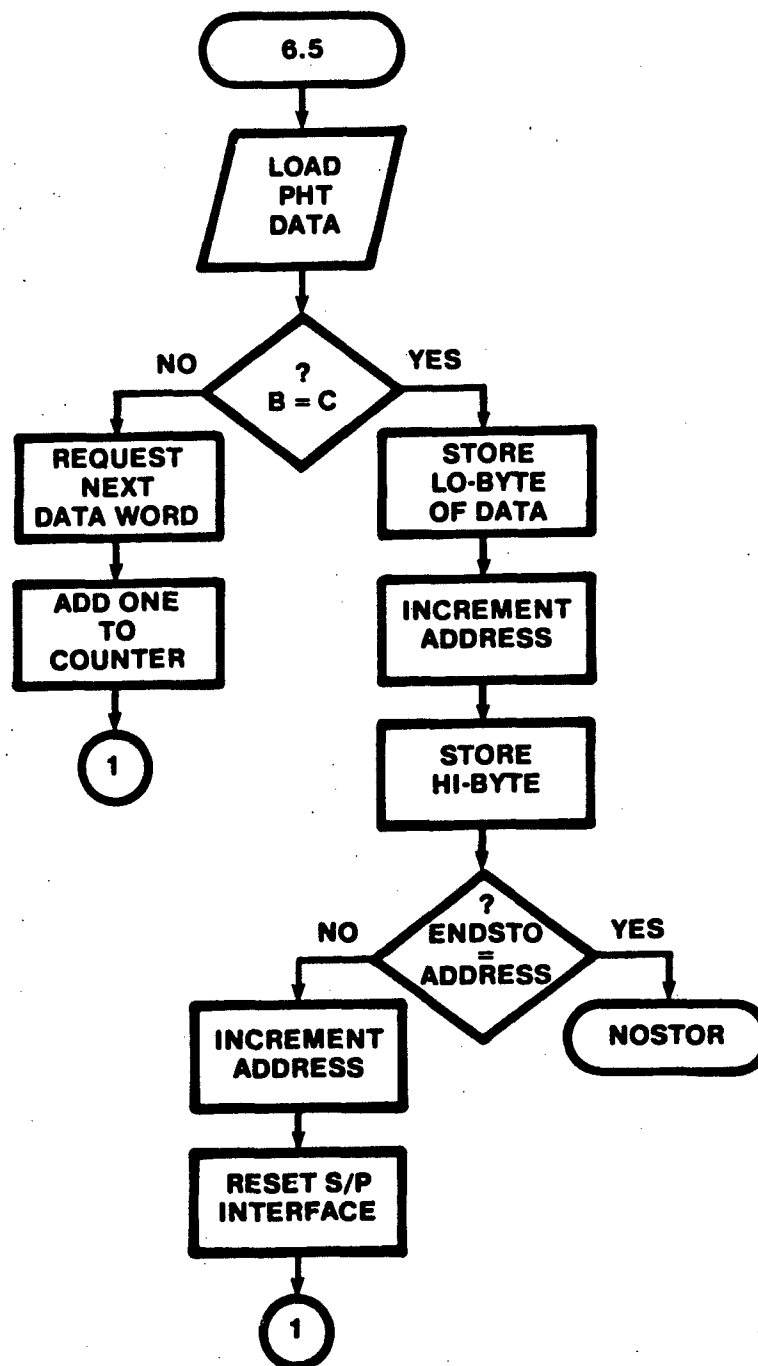
51 \$TITLE ('PHTMAP')
52 \$EJECT

PHTMAP

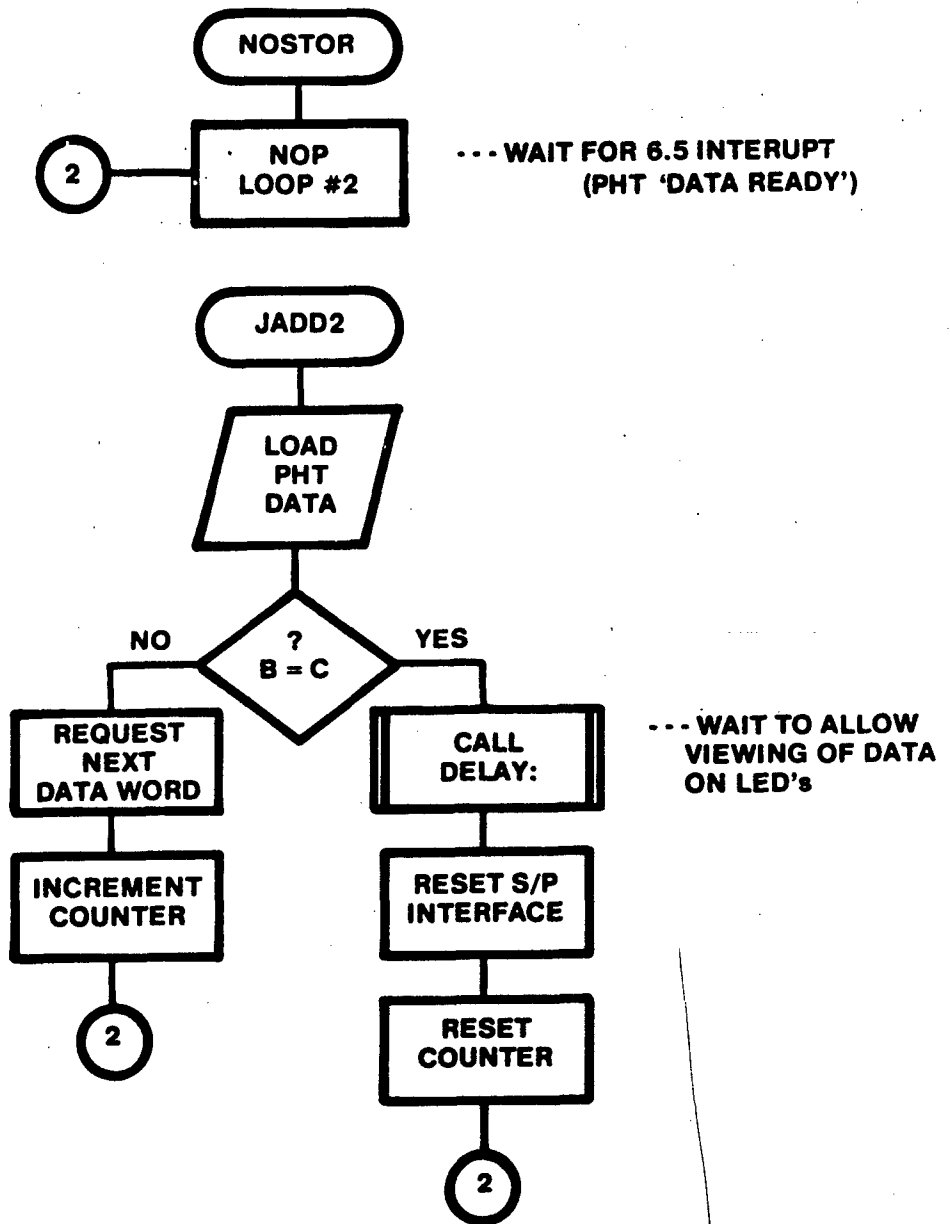


*-NOTE
 TO SELECT ONE OF THE THREE ANGLES (YAW, PITCH, ROLL), A CONSTANT
 MUST BE LOADED INTO REGISTER C BEFORE RUNNING PHTMAP INDICATING
 THE ANGLE DESIRED ACCORDING TO:
 00HEX - YAW DATA
 01HEX - PITCH DATA
 03HEX - ROLL DATA

PHTMAP CONT.



PHTMAP CONT.



NAVTRAEQUIPCEN IH-338

IS15-11 0000/0005 MACRO ASSEMBLER, V3.0
PMTAP

PMTAP

LOC	OBJ	LINE	SOURCE STATEMENT	
		53	CSEG	
		54	PMTAP	
0000	F3	55	DI	;DISABLE INTERRUPTS
0001	310000	56	LXI SP,STK	;SET STACK POINTED
		57		
0004	320000	58	STA RSTSP	;RESET SERIAL TO PARALLEL BOARD
		59		
0007	0600	60	MVI B,00H	;INITIALIZE COUNTER (B) TO ZERO
		61		
0009	210000	62	LXI H,FIRST	; (H,L) CONTAINS DI JMP INSTRUCTIONS
000C	220000	63	SHLD RST638	;STORE 1ST PART OF 6.5 INSTR
000F	212000	64	LXI H,JR001	; (H,L) CONTAINS ADDRESS FOR JUMP
0012	220000	65	SHLD RST63A	;STORE 6.5 JUMP ADDRESS
		66		
0015	110028	67	LXI D,BEGIN	; (D,E) CONTAINS 1ST STORAGE LOCATION
		68		
		69	NOP1	; *** LOOP #1 ***
		70		
0018	00	71	NOP	
0019	3E1D	72	MVI A,MASK	;UNMASK 6.5 INTERRUPT
001B	30	73	SIM	
001C	FB	74	EI	;ENABLE INTERRUPTS
001D	C31000	75	JMP NOP1	; ** WAIT FOR 6.5 INTERRUPT **
		76		
		77	JR001	
0020	2A0000	78	LHLD HINPUT	; (H,L) GETS INPUT (PULLS DOWN 6.5)
0023	78	79	MOV A,B	
0024	B9	80	CMP C	;DOES B = C ?
0025	CA2F00	81	JZ STORE	; IF EQUAL, STORE INPUT
		82		
0028	320000	83	STA GETELY	; IF NOT EQUAL, REQUEST NEXT WORD OF DATA
002B	C601	84	ADI 01H	; THEN - ADD 1 TO COUNTER
002D	47	85	MOV B,A	; AND
002E	C9	86	RET	; RETURN TO NOP1 LOOP
		87		
		88	STORE	
002F	EB	89	XCHG	; (D,E) CONTAINS INPUT ; (H,L) CONTAINS
		90		MEMORY ADDRESS
0030	73	91	MOV M,E	;STORE LO-BYTE OF INPUT
0031	23	92	INX M	;MEM = MEM + 1
		93		
0032	7A	94	MOV A,D	;ACC GETS HI-BYTE OF INPUT
0033	17	95	RAL	
0034	3F	96	CMC	
0035	1F	97	RAR	;COMPLIMENT MSB OF INPUT
0036	77	98	MOV M,A	;AND STORE IN MEMORY
		99		
0037	3EFF	100	MVI A,ENDSTO	;CHECK FOR END OF STORAGE
0039	BD	101	CMP L	; DOES REG L EQUAL END ?
003A	CA4500	102	JZ NOSTOR	; IF EQUAL, GO TO NOSTORE MODE
		103	\$EJECT	

NAVTRAEQUIPCEN IH-338

IS15-11 8888/8885 MACRO ASSEMBLER, V3 8
PMTAPP

PMTAPP

LOC	OBJ	LINE	SOURCE STATEMENT	
		104 ;		IF NOT EQUAL (SET UP FOR MORE STORAGE)
0030 23		105	INX H	MEM = MEM + 1
003E EB		106	XCHG	(D,E) POINTS TO MEMORY
		107 ;		
003F 320000	E	108	STA RSTSP	RESET SERIAL TO PARALLEL BOARD
		109 ;		
0042 0600		110	MVI B, 00H	RESET COUNTER TO ZERO
0044 C9		111	RET	RETURN TO NOP1 LOOP
		112 ;		
		113 NOSTOR:		
0045 00		114	NOP	
0046 215000	C	115	LXI H, JAD02	(H,L) GETS NEW JUMP ADD FOR 6.5
0049 220000	E	116	SHLD RST65A	AND THEN IS MOVED TO 6.5 RESTART AREA
		117 ;		
004C E1		118	POP H	REMOVE NOP1 RETURN ADDRESS
		119 ;		
0040 0600		120	MVI B, 00H	RESET COUNTER TO ZERO
		121 ;		
004F 320000	E	122	STA RSTSP	RESET SERIAL TO PARALLEL BOARD
		123 ;		
		124 NOP2:		*** LOOP #2 ***
0052 00		125	NOP	
0053 3E1D		126	MVI A, MASK	UNMASK 6.5 INTERRUPT
0055 30		127	SIM	ENABLE INTERRUPTS
0056 FB		128	EI	** WAIT FOR 6.5 INTERRUPT **
0057 C35200	C	129	JMP NOP2	
		130 ;		
		131 JAD02:		
005A 2A0000	E	132	LHLD HINPUT	(H,L) GETS INPUT FROM PMT
005D 78		133	MOV A, B	
005E B9		134	CMP C	DOES B = C ?
005F CA6900	C	135	JZ DISPLAY	IF EQUAL, WAIT BEFORE RESETTNG
		136 ;		
0062 320000	E	137	STA GETELV	IF NOT EQUAL, REQUEST NEXT WORD OF DATA
0065 C601		138	ADI 01H	
0067 47		139	MOV B, A	INCREMENT COUNTER
0068 C9		140	RET	AND RETURN TO NOP2 - LOOP #2
		141 ;		
		142 DISPLAY:		
0069 110020		143	LXI D, COUNT	(D,E) CONTAINS DELAY COUNT
006C CDF105		144	CALL DELAY	WAIT SPECIFIED TIME PERIOD
		145 ;		
006F 320000	E	146	STA RSTSP	RESET SERIAL TO PARALLEL BOARD
		147 ;		
0072 0600		148	MVI B, 00H	RESET COUNTER
0074 C9		149	RET	RETURN TO NOP2 - LOOP #2
		150 ;		
		151 REJECT		

NAVTRAEQUIPCEN IH-338

ISIS-II 8080/8085 MACRO ASSEMBLER, V3.0 PHTMAP
PHTMAP

LOC	OBJ	LINE	SOURCE STATEMENT
		152	END

PUBLIC SYMBOLS

EXTERNAL SYMBOLS

FIRST E 0000	GETELY E 0000	HINPUT E 0000	RST658 E 0000	RST65A E 0000	RSTSP E 0000	STK E 0000
--------------	---------------	---------------	---------------	---------------	--------------	------------

USER SYMBOLS

BEGIN A 2000	COUNT A 2000	DELAY A 05F1	DSPLAY C 0069	ENDST0 A 00FF	FIRST E 0000	GETELY E 0000
HINPUT E 0000	JADD1 C 0020	JADD2 C 005A	MASK A 001D	NOP1 C 0018	NOP2 C 0052	NOSTOR C 0045
PHTMAP C 0000	RST658 E 0000	RST65A C 0000	RSTSP E 0000	STK E 0000	STORE C 002F	

ASSEMBLY COMPLETE. NO ERRORS

NAVTRAEQUIPCEN IH-338

ISIS-II 8080/8085 MACRO ASSEMBLER, V3 0
FIFO

SUBS

LOC OBJ LINE SOURCE STATEMENT

```

493 ;
494 ;
495 ; *****
496 ; *
497 ; *   FIFO   *
498 ; *
499 ; *****
500 ;
501 ;

```

THIS SUBROUTINE IS USED TO SHIFT A TABLE CONTAINING DATA WORDS DOWN IN RAM OVERWRITING THE LAST WORD, BUT PRESERVING THE FIRST WORD. THE LENGTH OF THE WORDS INVOLVED IS CONSIDERED IN THE INPUT VALUES THAT ARE PASSED TO THIS SUBROUTINE.

FOR EXAMPLE, CONSIDER THIS TABLE CONTAINING THREE TWO-BYTE WORDS:

509 ; ADDRS TABLE

511 ; 2000H		W0-LO	2000H		W0-LO
512 ; 2001H		W0-HI	2001H		W0-HI
513 ; 2002H		W1-LO	2002H		W0-LO
514 ; 2003H		W1-HI	2003H		W0-HI
515 ; 2004H		W2-LO	2004H		W1-LO
516 ; 2005H		W2-HI	2005H		W1-HI

518 ; BEFORE
519 ; FIFO

AFTER
FIFO

(D,E) SHOULD CONTAIN THE ADDRESS OF W1-HI (2003H)
(H,L) SHOULD CONTAIN THE ADDRESS OF W2-HI (2005H)
B SHOULD CONTAIN THE LO-BYTE ADDRESS OF W0 (2000H)

526 ; INPUTS:

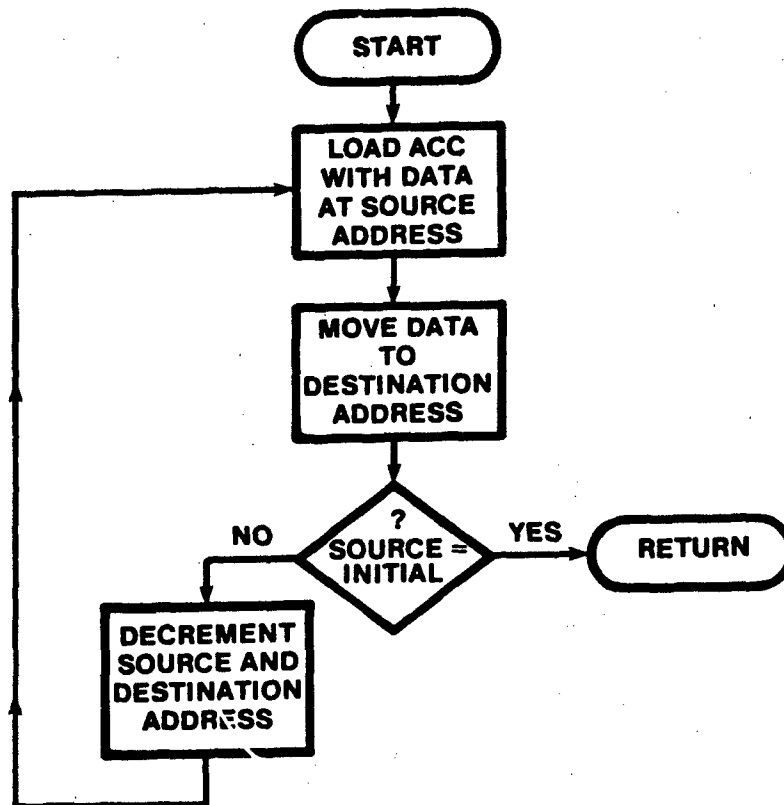
(D,E) - CONTAINS THE SOURCE ADDRESS (ADD. OF HI-BYTE OF NEXT TO LAST WORD)
(H,L) - CONTAINS THE ADDRESS OF THE HI-BYTE OF THE LAST WORD IN THE TABLE
B - CONTAINS THE ADDRESS OF THE FIRST TABLE LOCATION
** - THIS ROUTINE CANNOT SHIFT TABLES THAT CROSS HI-BYTE ADDRESS BOUNDARIES.

532 ; OUTPUT:

THE DESCRIBED TABLE IS SHIFTED.

534 ; EJECT

FIFO



INPUT: (D, E) ← SOURCE ADDRESS
 (H, L) ← DESTINATION ADDRESS
 B ← INITIAL ADDRESS

OUTPUT: TABLE IS SHIFTED DOWNWARDS IN RAM
 (NUMBER OF LOCATIONS MOVED IS
 IMPLIED BY DIFFERENCE BETWEEN
 SOURCE AND DESTINATION ADDRESSES)

NAVTRAEQUIPCEN IH-338

1515-II 8080/8085 MACRO ASSEMBLER, V3.0 SUBS
FIFO

LOC	OBJ	LINE	SOURCE STATEMENT
		535 ;	
		536	CSEG
		537	FIFO:
00C0	1A	538	LDAX D ; LOAD ACC WITH DATA AT SOURCE ADDRESS
00CE	77	539	MOV M, A ; MOVE SOURCE DATA DOWN TWO POSITIONS
		540 ;	
00CF	78	541	MOV A, B ; MOVE ADD OF FIRST WORD TO ACC
00D0	88	542	CMP E ; AND COMPARE WITH SOURCE ADDRESS
00D1	08	543	RZ ; RETURN IF FIRST WORD HAS BEEN MOVED
		544 ;	
00D2	18	545	DCX D ; IF MORE TO SHIFT, POINT TO NEXT SOURCE
00D3	28	546	DCX H ; AND DESTINATION ADDRESS
00D4	C3C000 C	547	JMP FIFO ; THEN SHIFT NEXT PIECE OF DATA
		548	\$EJECT

NAVTRAEQUIPCEN IH-338

IS15-II 8888/8885 MACRO ASSEMBLER, V3 0
TABLE_SET

SUBS

LOC	OBJ	LINE	SOURCE STATEMENT
		456 ;	
		457 ;	
		458 ;	*****
		459 ;	* * *
		460 ;	* TBLSET *
		461 ;	* * *
		462 ;	*****
		463 ;	
		464 ;	THIS SUBROUTINE IS USED TO FILL A GROUP OF RAM LOCATIONS WITH AN INITIAL VALUE
		465 ;	WORD WHICH IS TWO-BYTES LONG
		466 ;	
		467 ;	INPUTS:
		468 ;	(D,E) - CONTAINS THE INITIAL VALUE
		469 ;	(H,L) - CONTAINS THE FIRST ADDRESS FOR INITIALIZATION
		470 ;	ACC - LO-BYTE OF FINAL ADDRESS IN THE TABLE
		471 ;	** - TABLE CANNOT EXTEND ACROSS THE HI-BYTE BOUNDARY
		472 ;	
		473 ;	OUTPUT:
		474 ;	RAM LOCATIONS FROM THE FIRST ADDRESS TO THE FINAL ADDRESS ARE FILLED
		475 ;	WITH THE INITIAL VALUE IN (D,E)
		476 ;	
		477 ;	
		478	CSEG
		479	TBLSET:
00C4	73	480	MOV M,E ; MOVE LO-BYTE INITIAL VALUE TO (H,L) ADDRESS
00C5	23	481	INX H ; INCREMENT (H,L) ADDRESS
00C6	72	482	MOV M,D ; MOVE HI-BYTE INITIAL VALUE TO (H,L) ADDRESS
		483 ;	
00C7	80	484	CMP L ; CHECK FOR END OF TABLE
00C8	C8	485	RZ ; RETURN IF AT END OF TABLE
		486 ;	
00C9	23	487	INX H ; IF NOT AT END INCREMENT (H,L)
00CA	C3C400 C	488	JMP TBLSET ; INITIALIZE NEXT TWO BYTES
		489 ;	
		490 ;	
		491	\$TITLE ('FIFO')
		492	\$EJECT

NAVTRAEQUIPCEN IH-338

1515-II 8080/8085 MACRO ASSEMBLER, V3.0

SUBS

MAX

LOC	OBJ	LINE	SOURCE STATEMENT
		300 ;	
		301 ;	*****
		302 ;	* * *
		303 ;	* MAX *
		304 ;	* * *
		305 ;	*****
		306 ;	
		307 ;	
		308 ;	(THIS SUBROUTINE COMPARES A TWO-BYTE WORD WITH A ONE-BYTE WORD (MAX)
		309 ;	IF THE TWO-BYTE WORD IS GREATER THAN THE MAX WORD, THEN THE MAX
		310 ;	WORD IS RETURNED TO THE CALLING PROGRAM. IF THE TWO-BYTE WORD IS LESS
		311 ;	THAN THE MAX WORD, THEN THE LO-BYTE OF THE TWO-BYTE WORD IS RETURNED
		312 ;	TO THE CALLING PROGRAM.
		313 ;	
		314 ;	
		315 ;	INPUTS:
		316 ;	ACC - CONTAINS THE MAXIMUM VALUE (ONE-BYTE)
		317 ;	(H,L)- CONTAINS THE TWO-BYTE WORD FOR COMPARISON
		318 ;	
		319 ;	OUTPUT:
		320 ;	B - CONTAINS THE LESSOR OF THE MAXIMUM VALUE OR THE TWO-BYTE WORD
		321 ;	
		322 ;	
		323	CSEG
		324	MAX:
		325 ;	
0078	47	326	MOV B, A ; B GETS MAXIMUM VALUE
		327 ;	
0079	7C	328	MOV A, H ; ACC GETS HI-BYTE C-VALUE
007A	FE00	329	CPI 00H ; IF HI-BYTE IS NOT ZERO,
007C	C0	330	RNZ ; RETURN WITH MAX IN B
		331 ;	
007D	7D	332	MOV A, L ; ACC GETS LO-BYTE C-VALUE
007E	B8	333	CP B ; COMPARE WITH MAXIMUM
007F	D0	334	RNC ; RETURN IF L IS GREATER THAN MAXIMUM
		335 ;	
0080	45	336	MOV B, L ; ELSE MOVE L TO B
0081	C9	337	RET ; RETURN WITH LESSOR VALUE IN B
		338 ;	
		339 ;	
		340	\$TITLE ('STORE1')
		341	\$EJECT

NAVTRAEQUIPCEN IH-338

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NAVTRAEQUIPCEN IH-338

APPENDIX B

RHMC HARDWARE

An Intel SDK-85 development board is used as the micro-controller for the RHMC system -- primarily because it provides a ready-made micro system at a reasonable cost. The microprocessor is an Intel 8085A, which is capable of addressing only 512 bytes of RAM, 2000 bytes of monitor ROM and 2000 bytes of Erasable Programmable Read Only Memory (EPROM). The 8085A is in communication with an in-house designed board which provides two digital to analog converter (DAC) channels for raster shift, EPROM for RHMC program storage, address decoders, and vertical sync for both the Polhemus Head Tracker (PHT) and the microprocessor. In addition, the system contains the Polhemus head tracker (PHT) data controller which allows head pointing direction (HPD) data transfer from the PHT to the microprocessor, and a separate data buffer board than enables the CIG system to take in HPD data transparent to the operation of the 8085 microprocessor system. Figure B1 shows a block diagram of the RHMC and interface hardware.

The PHT data controller (see schematic and timing diagram) controls the format and the distribution of Head Pointing Direction data from the Polhemus Head Tracker. About 15.5 ms. after the sync signal (vertical sync) is sent to the PHT, initiating its position sampling sequence, the PHT indicates that the data is ready by sending, appropriately, a "data ready" pulse to the data controller. The PHT orientation and positional data is then ready to be clocked out of the serial port. A "data acknowledge" signal is returned to the PHT by the controller and a 500 kHz. burst consisting of 17 clock pulses is also sent which clocks out the first 17-bit word, "yaw." This serial string of bits is clocked into dual, 10-bit, serial in, parallel out shift registers. At the end of the 17th clock pulse, the clock is inhibited, and the first 16 bits of the 17-bit word are transferred to dual 8-bit data buffers. These buffers, when full, send an interrupt (Rst. 6.5) to the 8085 microprocessor. The micro, meanwhile, has been patiently waiting in a loop for the data. Upon receipt of the Rst. 6.5 interrupt, the micro addresses the buffers and pulls the data into memory for future processing. The micro writes to memory location (8xx2) which sends a "get data" pulse to the controller and the micro returns to the loop to await further data. Again, the controller sends out a burst of 17 pulses, clocking in the next word, "pitch." In the same sequence as before, the 8085 stores this next word and requests the roll data. At the end of this sequence, "data acknowledge" is cleared and the 8085 begins the computation cycle which eventually determines the 8-bit values sent to the horizontal and vertical, raster shifting, digital to analog converters (HDAC and VDAC). These values are latched into the DACs during the vertical retrace of the laser video projector. Vertical sync (or retrace) is acknowledged as a 7.5 interrupt by the microprocessor.

Again returning to the system block diagram in Figure B1, the offset signals from the HDAC and VDAC are routed to summing circuits; a summer feeding the VCO for the horizontal shift, and a summing point within the scanner controller for the vertical shift.

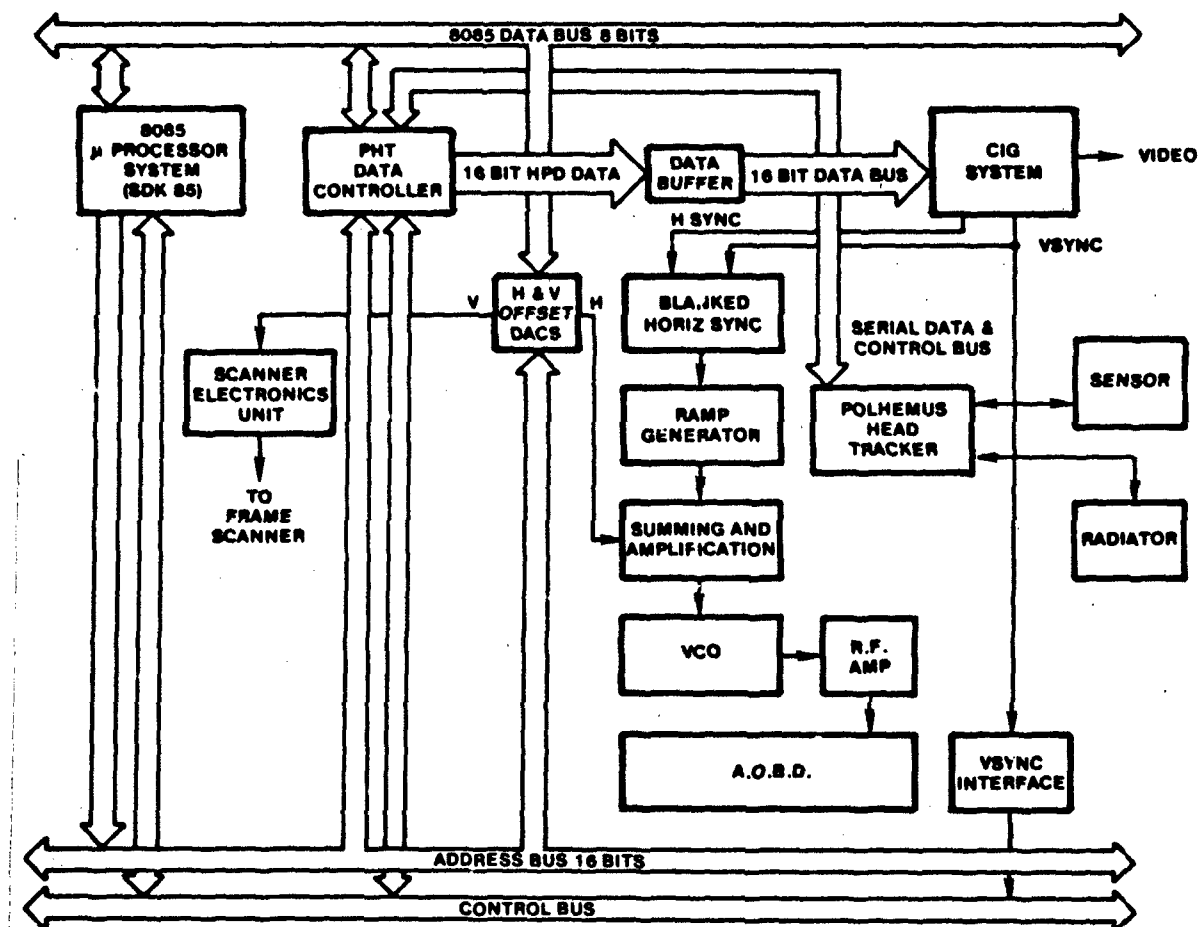


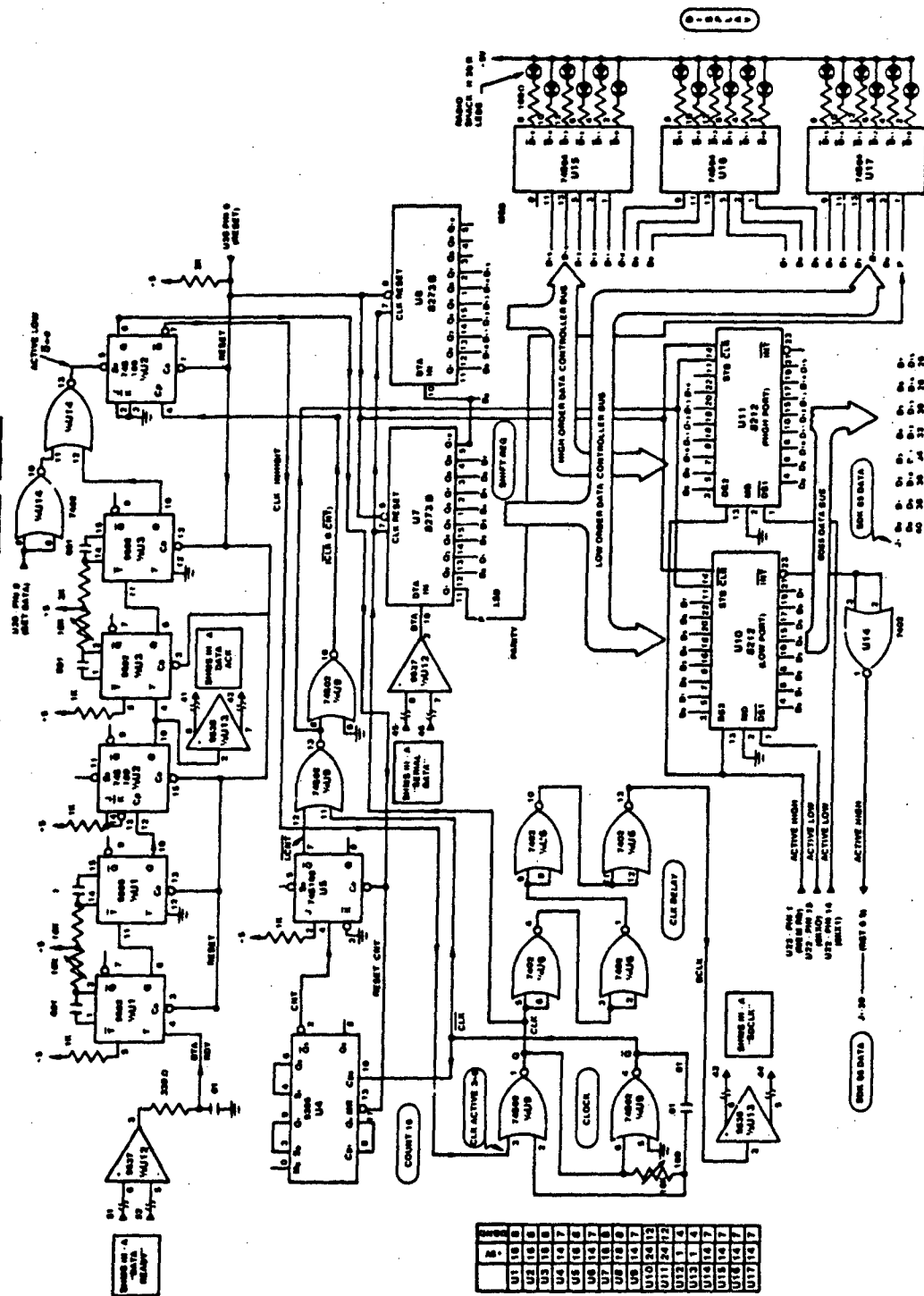
Figure B1. RHMC and Interface Hardware.

The horizontal offset signal from the HDAC is summed with the output of the ramp generator. The voltage shift of this signal frequency shifts the voltage controlled oscillator which outputs a frequency chirp centered at 375 MHz. Spanning some 200 MHz., the frequency chirp can be shifted up or down in frequency as much as 25 MHz. After suitable amplification, the Acousto Optic Beam Deflector (AOBD) receives the shifted chirp and shifts the horizontal line scan accordingly. The voltage controlled oscillator (VCO) is required to output a chirp, or frequency sweep at a horizontal line rate. As previously mentioned, the VCO is a non-linear device when operated at these line rates (15 to 30 kHz.). Since the VCO is non-linear, its driving signal must be carefully selected and conditioned to achieve a linear output, i.e., a linear frequency chirp. A linear frequency chirp applied to the AOBD results in a sharply focused, linear horizontal sweep. The task of providing a linear frequency chirp is difficult enough; providing a signal which produces a shiftable linear frequency chirp at the output of the VCO proved to be impossible. The subsequent non-linearity produces noticeable display distortion, reducing both the resolution and linearity of the display.

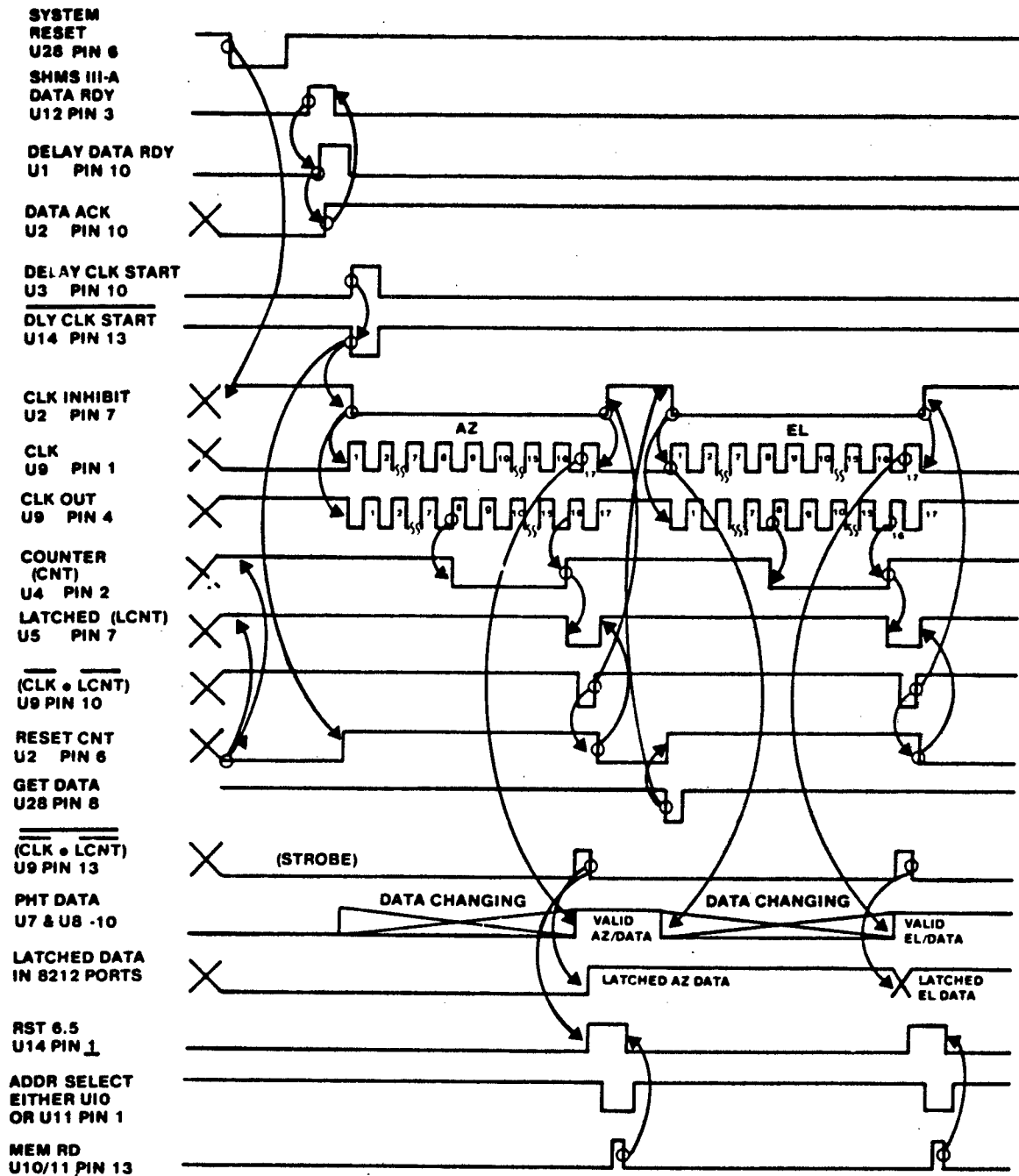
A minor modification of the scanning controller, which drives the frame scanner, allows the vertical offset signal from the VDAC to shift the angle at which the frame scanner begins its vertical scan. This provides the required vertical raster shift.

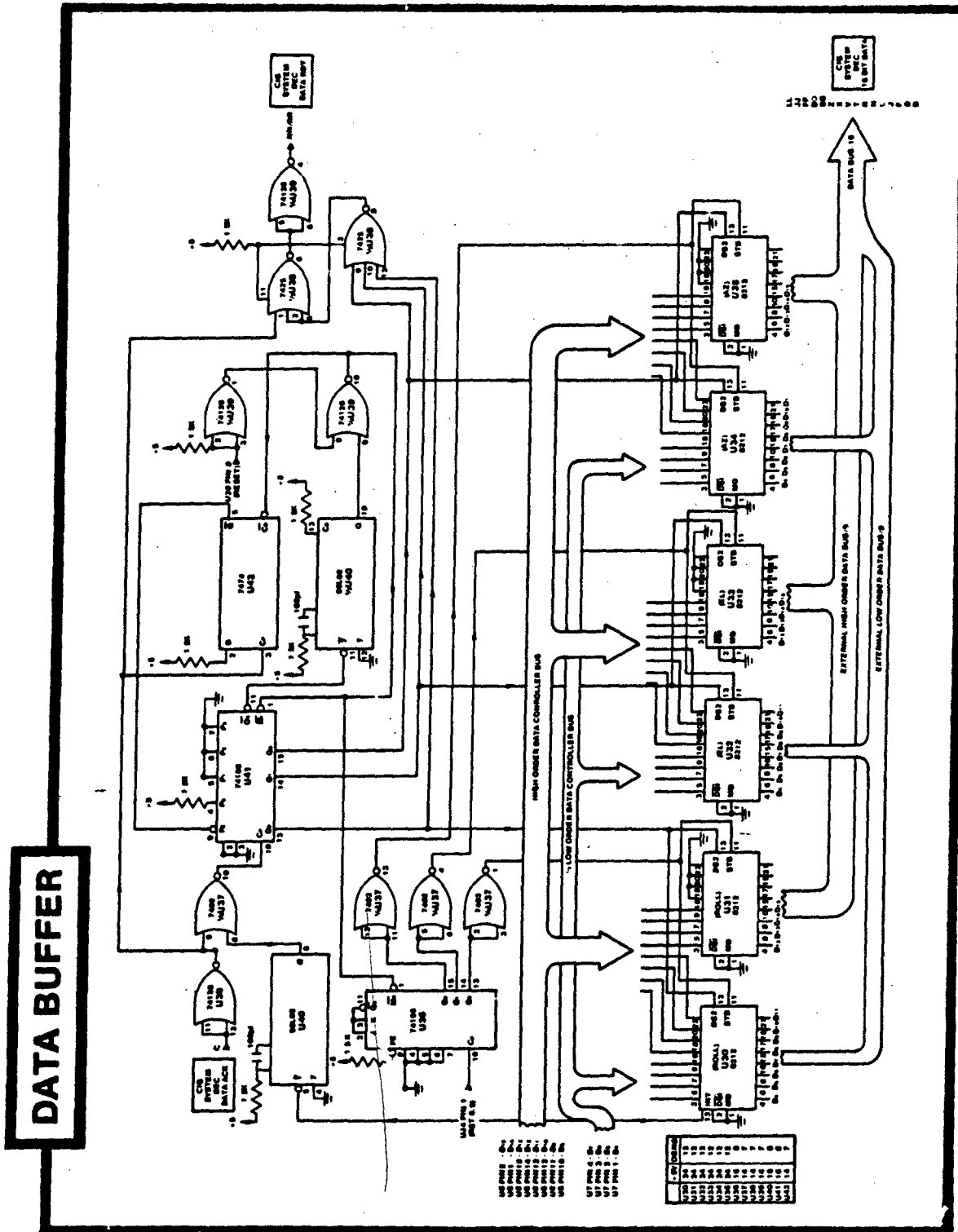
Both the CIG and RHMC system require head pointing direction (HPD) data every field (16.7 ms.). The data buffer (see schematic and timing diagram) allows the CIG to take in HPD data relatively independent of the operation of the RHMC system. It holds the pitch, roll and yaw data until the CIG sends a request for data. Basically, the data buffer counts the number of Rst. 6.5 interrupts emitted by the PHT data controller and loads one of three 16-bit buffers on each rising edge. When the third buffer has been loaded with data from the PHT data controller bus, a "data ready" is sent to the CIG system indicating that a complete set of HPD data is ready to be transferred, and the first data word, azimuth, is placed on the 16-bit CIG/buffer bus. When the CIG system accepts the data, it returns a "data acknowledge," which places the next data word, elevation, on the bus. This action, in turn, sends another "data ready" to the CIG system. When the final data word, roll, is received by the CIG, and a "data acknowledge" is returned, the three buffers are cleared. The data buffer is then ready for another set of HPD data.

PHT (SHMS III-A) DATA CONTROLLER

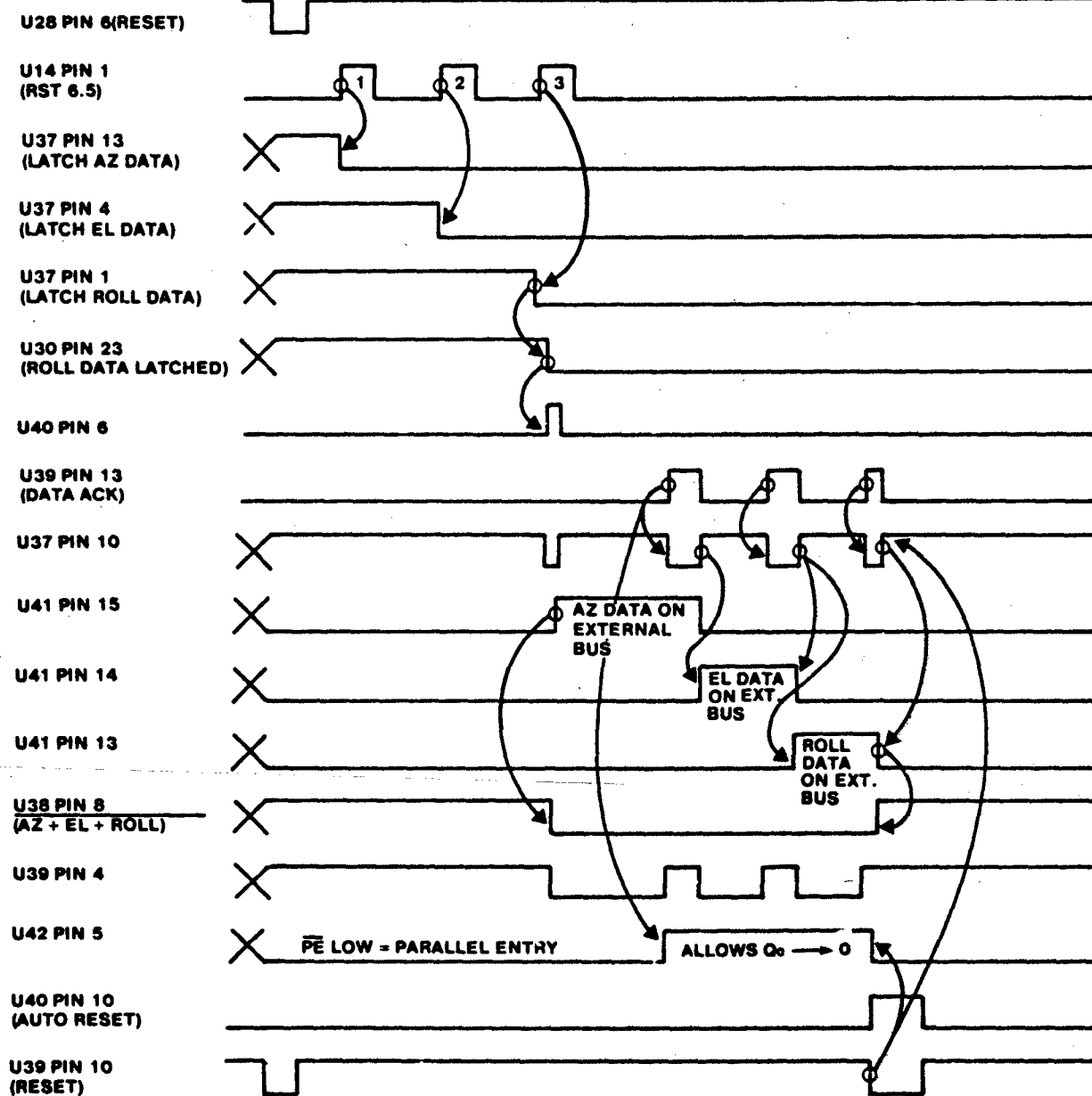


PHT (SHMS III) DATA CONTROLLER TIMING DIAGRAM



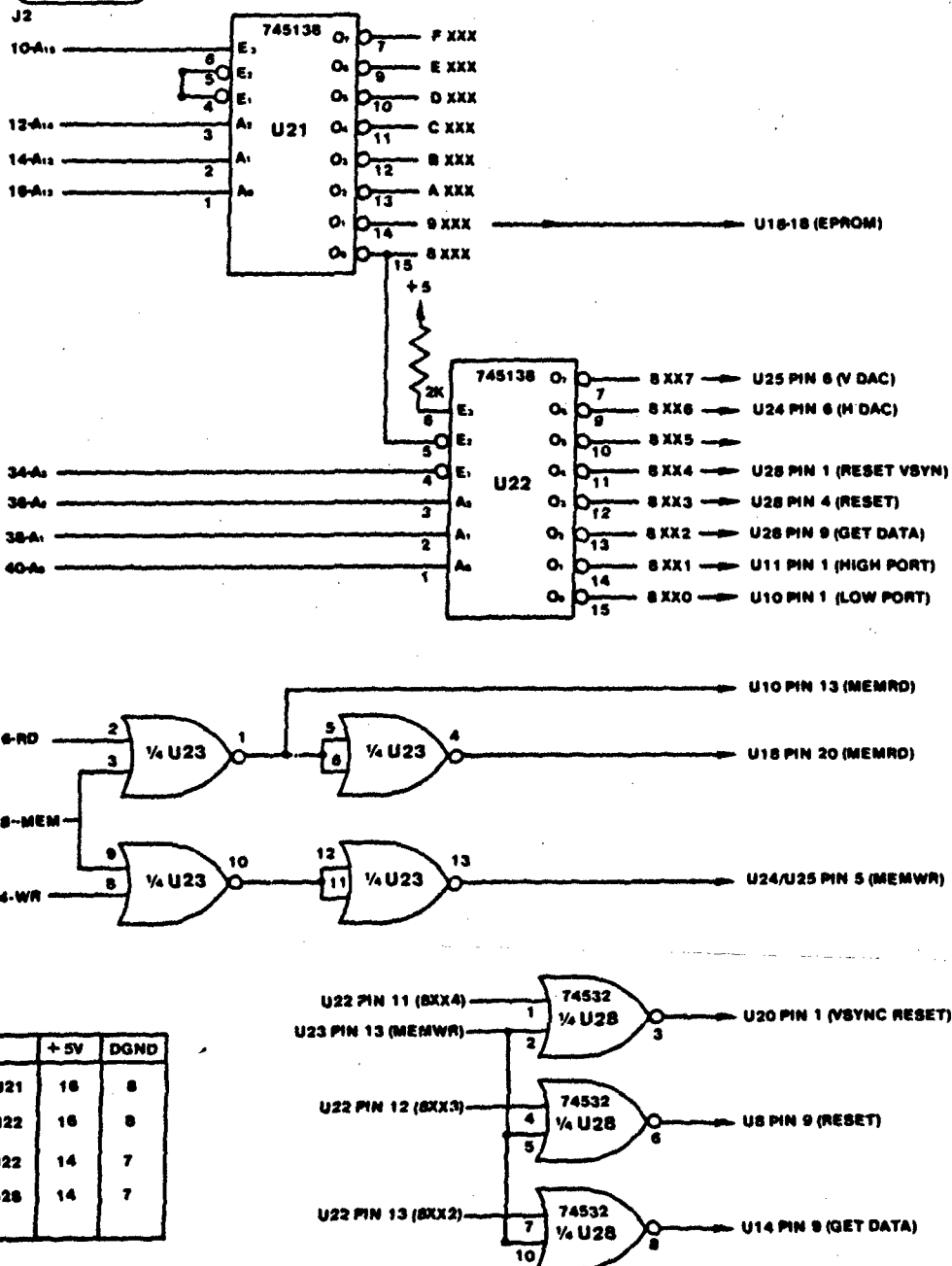


DATA BUFFER TIMING DIAGRAM

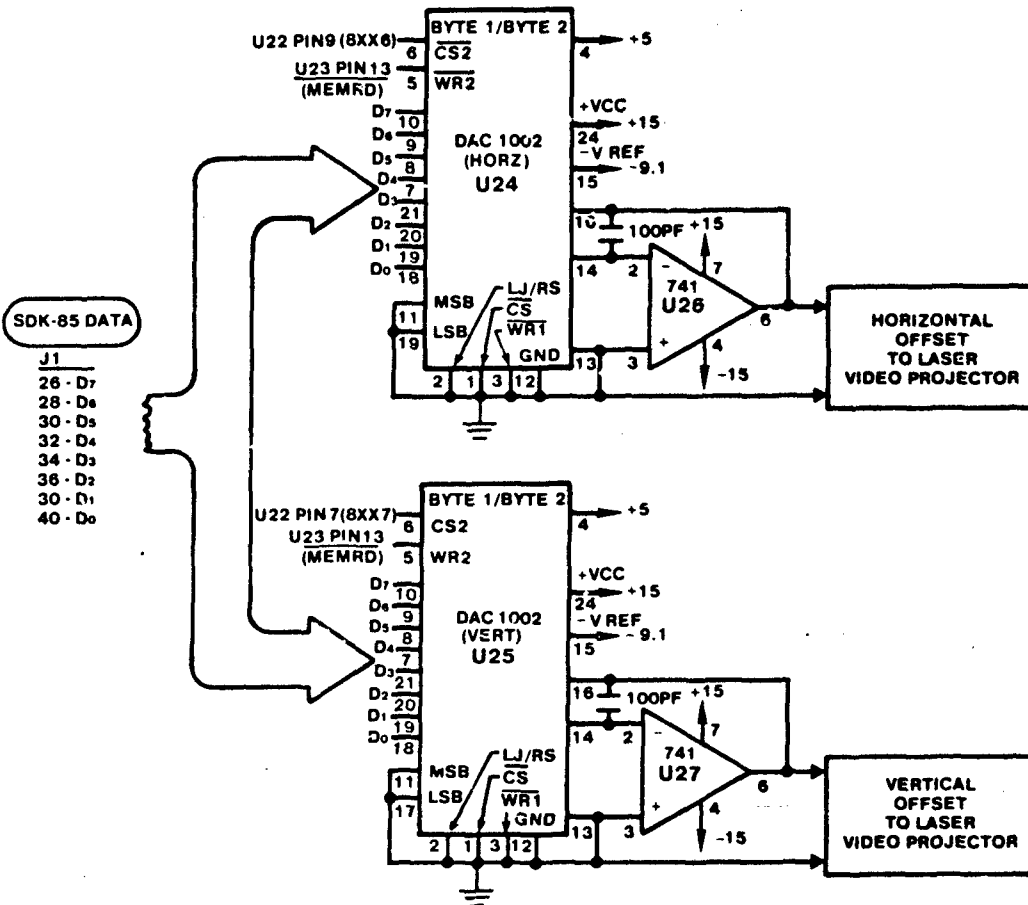


ADDRESS DECODE AND CONTROL

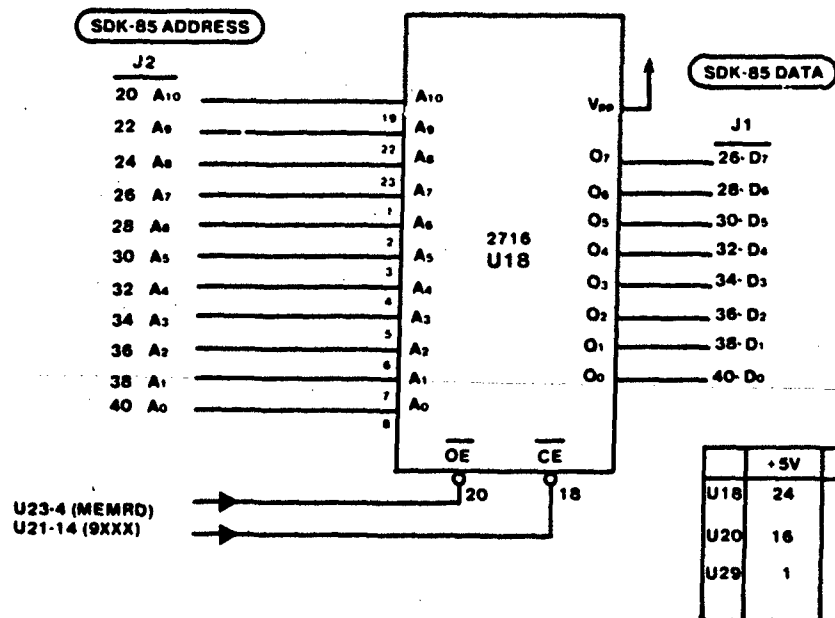
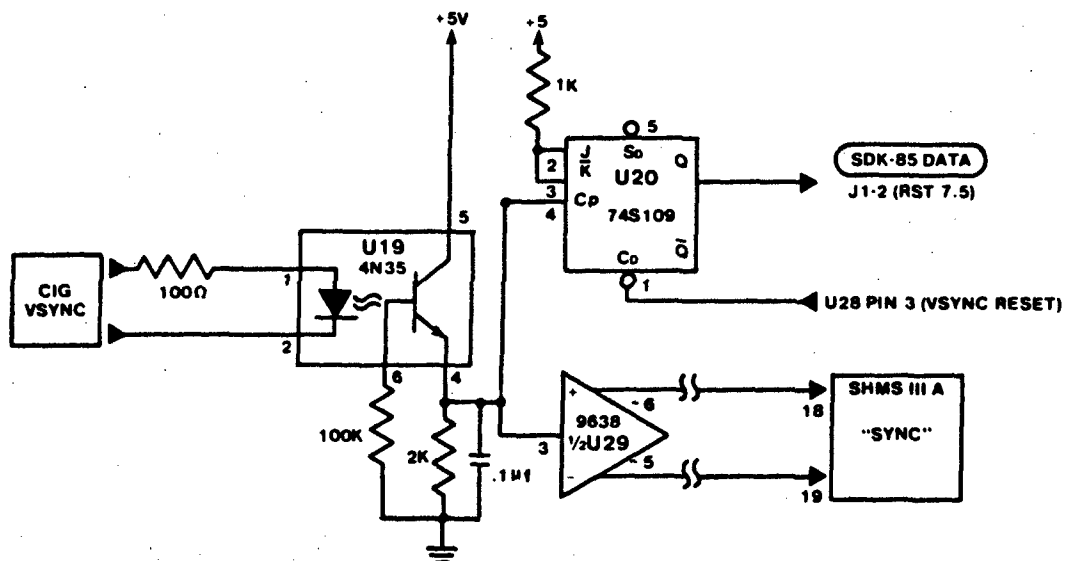
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